

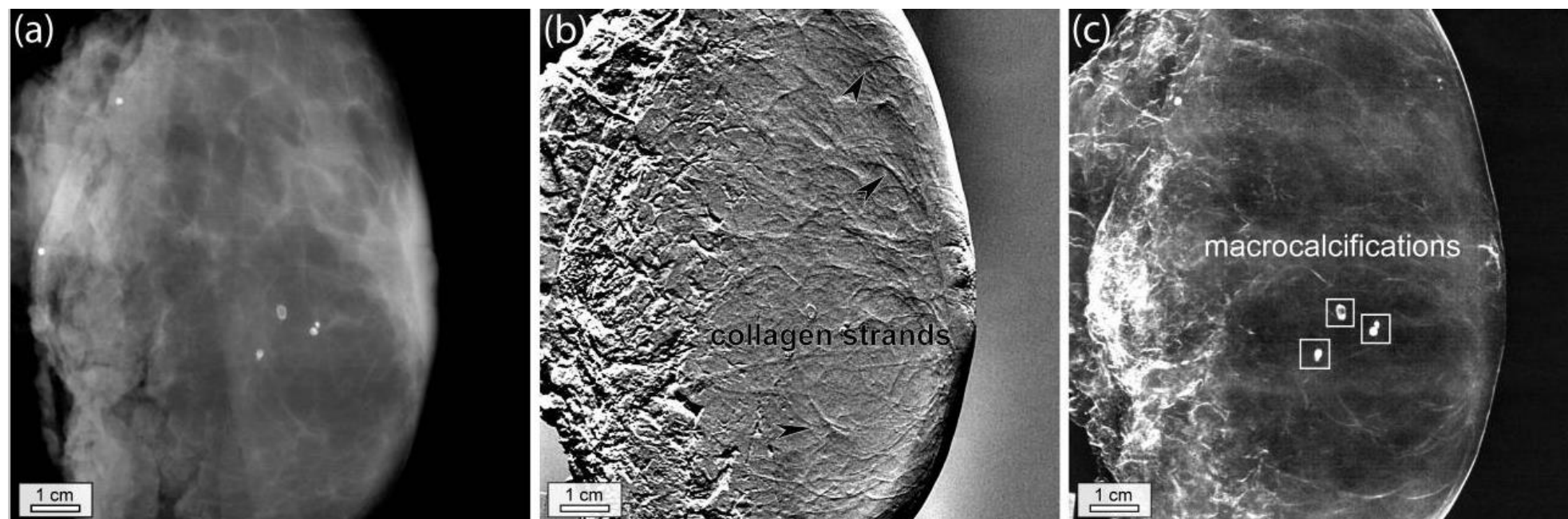
Masks for alternative X-ray imaging

David Jurado

APLICACIONES INTERDISCIPLINARIAS DE DETECTORES DE PARTÍCULAS

Universidad de los Andes

Conventional X-ray imaging relies on the absorption of X-rays by different tissues, which can result in low-contrast images. A solution to this issue is detecting DPC and DF due to interactions of photons with matter, which is highly sensitive for low-attenuating tissues and samples.



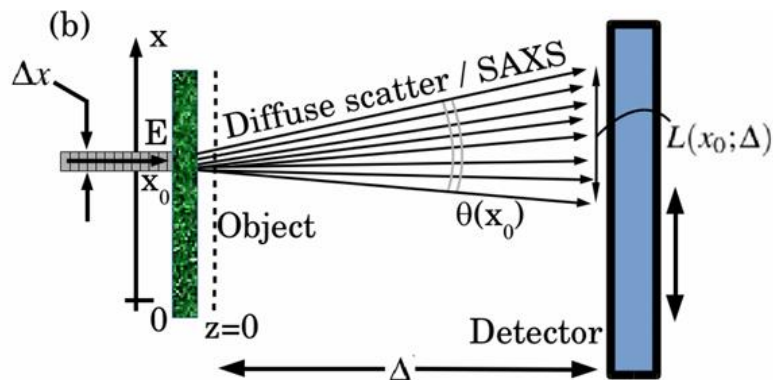
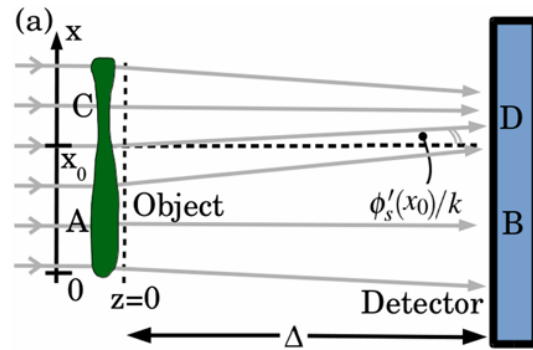
[1]

IT IS CRUCIAL TO MAKE ALTERNATIVE X RAY IMAGING ACCESSIBLE

Aplicaciones interdisciplinarias de detectores de partículas

Light transport approach

Based on [2], The X-ray Fokker-Planck equation is a modified version of the Transport of Intensity Equation



Second order (below the detector resolution)

$$\mathcal{J}_\perp = \mathcal{J}_\perp^{(1)} + \mathcal{J}_\perp^{(2)}$$

$$\mathcal{J}_\perp^{(1)} = \frac{I \nabla_\perp \phi}{k}$$

Transverse Poynting vector

$$\mathcal{J}_\perp^{(2)} = -\nabla_\perp (D I)$$

Diffusive energy transport

$$\mathcal{J}_\perp = [1 - F(\mathbf{r})] \mathcal{J}_\perp^{(1)} + F(\mathbf{r}) \mathcal{J}_\perp^{(2)}$$

$$\frac{\partial I}{\partial z} = -\nabla_{\perp} \cdot \mathcal{J}_{\perp}$$

$$\frac{\partial I}{\partial z} = -\nabla_{\perp} \cdot [1 - F(\mathbf{r})] \mathcal{J}_{\perp}^{(1)} + F(\mathbf{r}) \mathcal{J}_{\perp}^{(2)}$$

Since the fraction of energy converted to small angle scattering in X-rays $F(\mathbf{r}) \ll \mathbf{1}$

Then $1 - F(\mathbf{r}) \approx 1$

$$\frac{\partial I}{\partial z} = -\nabla_{\perp} \cdot \left[\frac{I \nabla_{\perp} \phi}{k} - F \nabla_{\perp} (DI) \right]$$

F varies slowly enough so $\nabla_{\perp} \cdot [F \nabla_{\perp} (DI)] \approx F \nabla_{\perp}^2 (DI)$ Yielding the Fokker-Planck equation

$$\frac{\partial I(x, y, z)}{\partial z} = -\nabla_{\perp} \cdot \left[\frac{I(x, y, z) \nabla_{\perp} \phi(x, y, z)}{k} \right] - F(x, y, z) \nabla_{\perp}^2 (D(x, y, z) I(x, y, z))$$

For a small propagation distance

$$I(\mathbf{r}, z) = I(\mathbf{r}, 0) + z \left. \frac{\partial I}{\partial z} \right|_{z=0}$$

$$I(\mathbf{r}, z) = I(\mathbf{r}, 0) - \frac{z}{k} \nabla_{\perp} \cdot (I(\mathbf{r}, 0) \nabla_{\perp} \phi(\mathbf{r}, 0)) + z F(\mathbf{r}) D(\mathbf{r}) \nabla_{\perp}^2 I(\mathbf{r}, 0)$$

Given $S(\mathbf{r}) = F(\mathbf{r}) D(\mathbf{r})$ as the sample scattering coefficient and the setup intensity as $I(\mathbf{r}, 0) = T(\mathbf{r}) M(\mathbf{r})$ Then the measured intensity for a pixel detector is

$$I = \int_A I(\mathbf{a}, z) da$$

For a single row this is:

$$I_n = T(x_n) \int_{x_n}^{x_{n+1}} M(x) dx - \frac{z}{k} T(x_n) \nabla_{\perp}^2 \phi(x_n) \int_{x_n}^{x_{n+1}} M(x) dx - \frac{z}{k} T(x_n) \partial_x \phi(x_n) \int_{x_n}^{x_{n+1}} M'(x) dx + z T(x_n) S(x_n) \int_{x_n}^{x_{n+1}} M'(x) dx$$

Then $T_n = T(x_n)$, $D_n = \frac{z}{k} \partial_x \phi(x_n)$ and $L_n = \frac{z}{k} \nabla_{\perp}^2 \phi(x_n)$

$$I_n = T_n \int_{x_n}^{x_{n+1}} M(x) dx - T_n L_n \int_{x_n}^{x_{n+1}} M(x) dx - T_n D_n \int_{x_n}^{x_{n+1}} M'(x) dx + z T_n S(x_n) \int_{x_n}^{x_{n+1}} M''(x) dx$$

$$I_n = T_n \int_{x_n}^{x_{n+1}} M(x) dx (1 - L_n) - T_n D_n \int_{x_n}^{x_{n+1}} M'(x) dx + z T_n S_n \int_{x_n}^{x_{n+1}} M''(x) dx$$

Now defining $\int_{x_n}^{x_{n+1}} M(x) dx = \mathcal{M}_n$, $\int_{x_n}^{x_{n+1}} M'(x) dx = \mathcal{M}'_n$ and $z \int_{x_n}^{x_{n+1}} M''(x) dx = \mathcal{M}''_n$

$$I_n = T_n (1 - L_n) \mathcal{M}_n - T_n D_n \mathcal{M}'_n + T_n S_n \mathcal{M}''_n$$

Where $\mathcal{M}_n, \mathcal{M}'_n, \mathcal{M}''_n$ are functions that depends on alignment, mask properties and wavefront markers.

Takeaways:

$$I_n = \underbrace{\mathcal{M}_n T_n (1 - L_n)}_{\text{Absorption channel}} - \underbrace{\mathcal{M}'_n T_n D_n}_{\text{DPC channel}} + \underbrace{\mathcal{M}''_n T_n S_n}_{\text{DF channel}}$$

Laplacian phase correction Differential phase Dark field USAXS

\mathcal{M}_n Is the sensibility of each channel in the image

Each column I_n acts like a bin for each signal, retrieval methods can then be used to extract each signal.

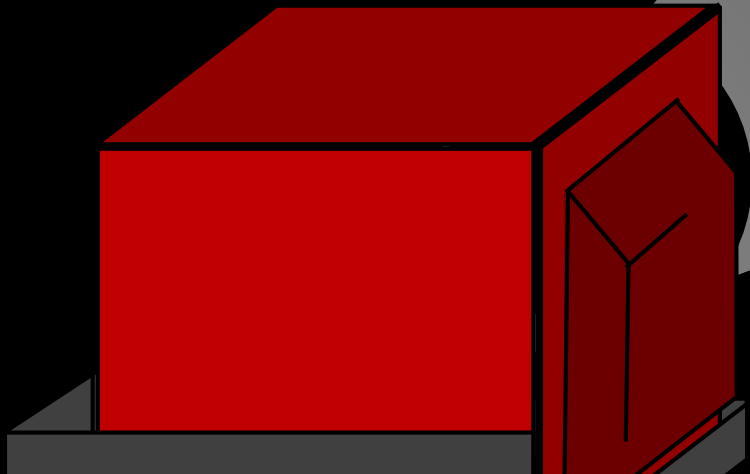
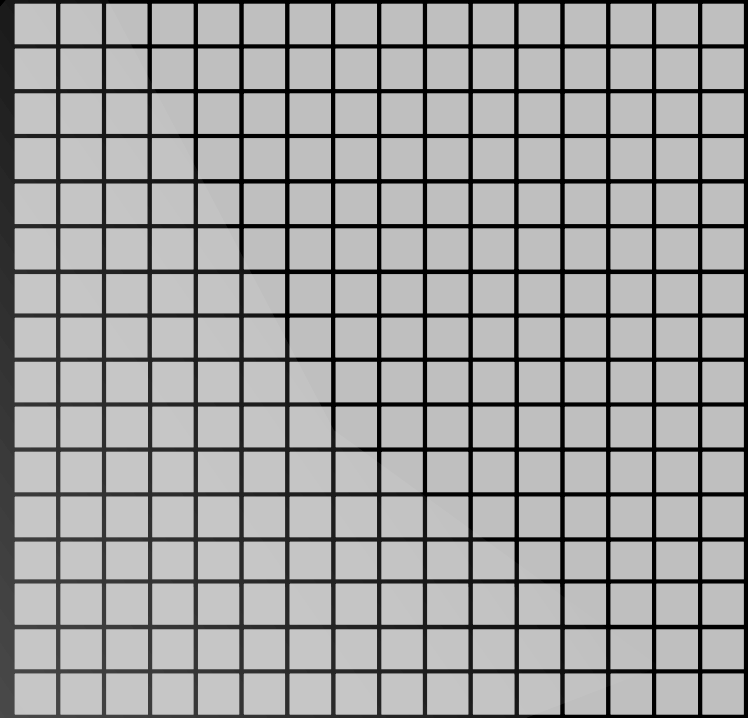
Edge Illumination
Phase

Contrast
Imaging

Edge Illumination

Phase

Contrast
Imaging

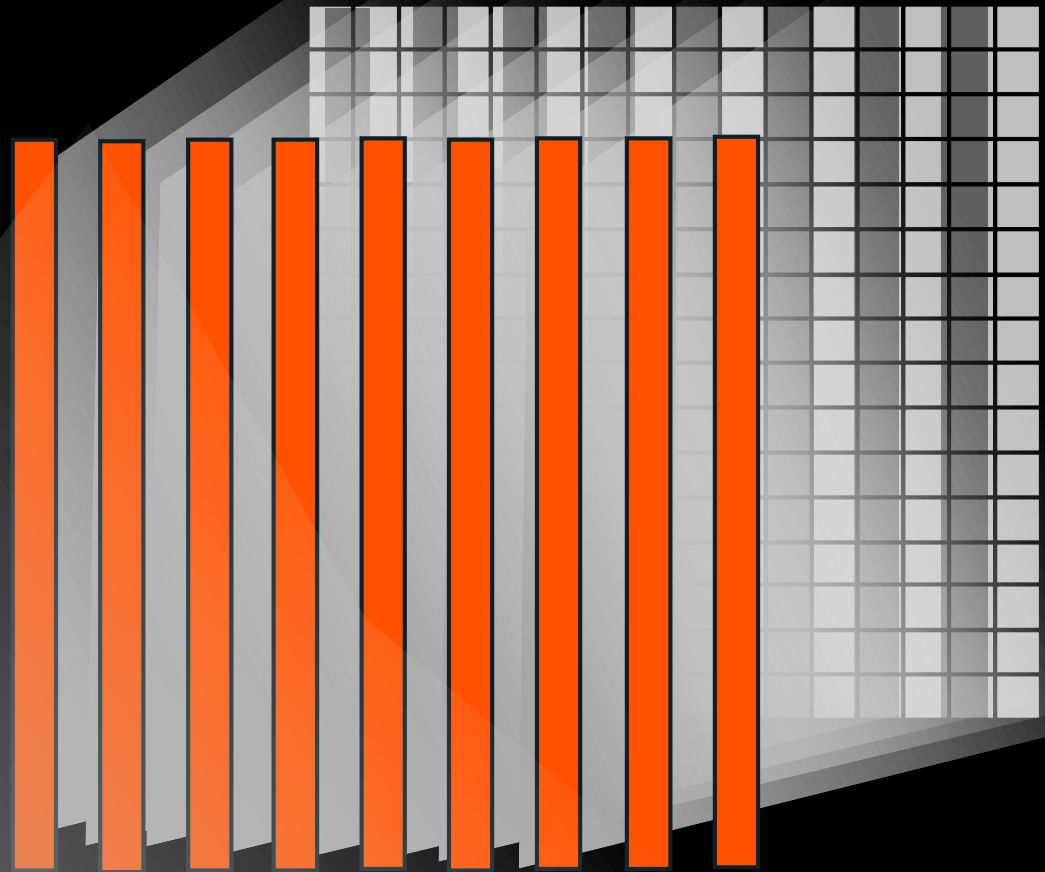


Aplicaciones interdisciplinarias de
detectores de partículas

Edge Illumination

Phase

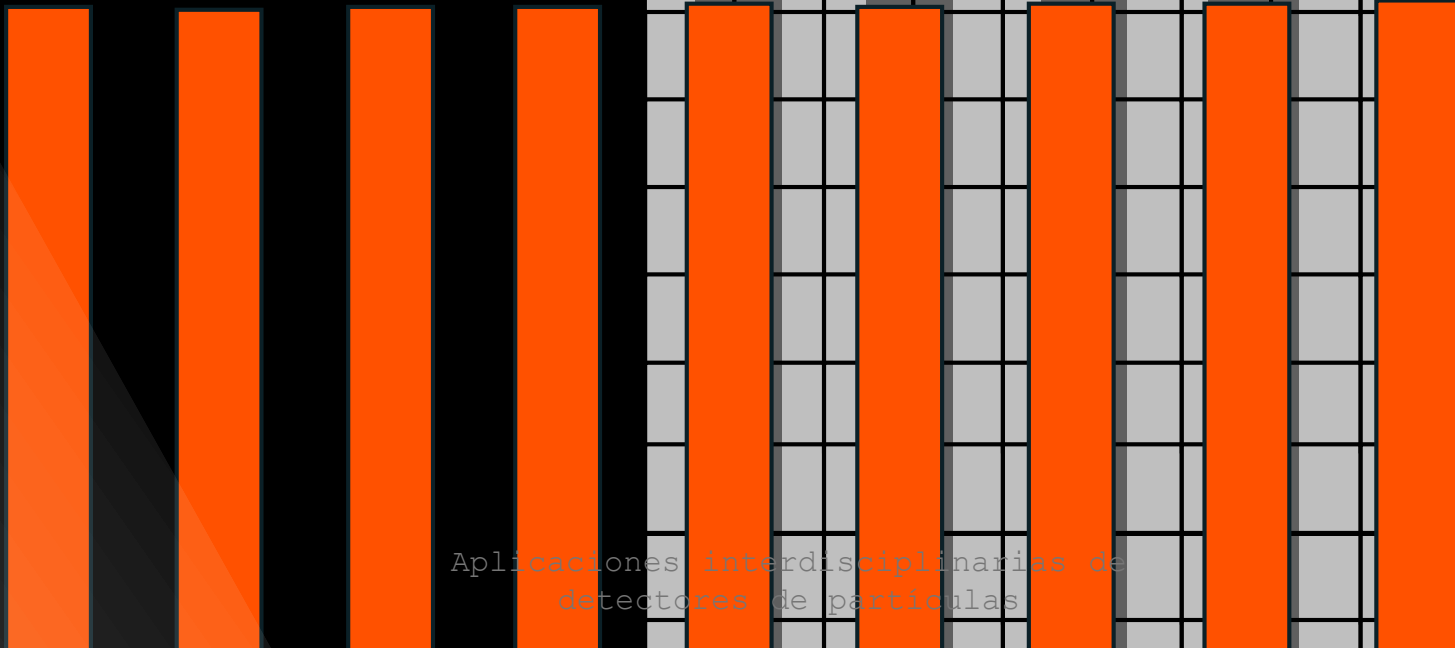
Contrast
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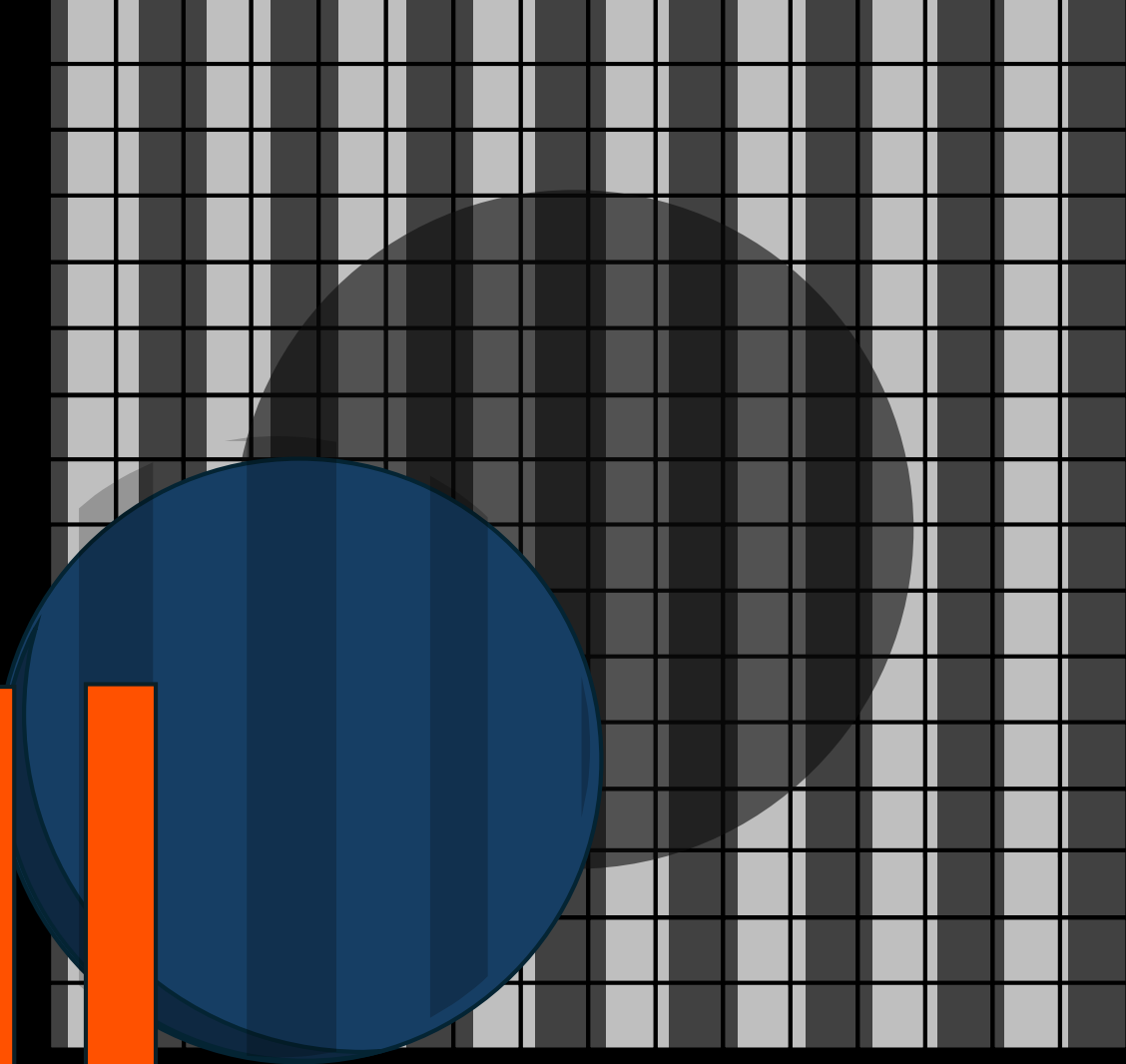


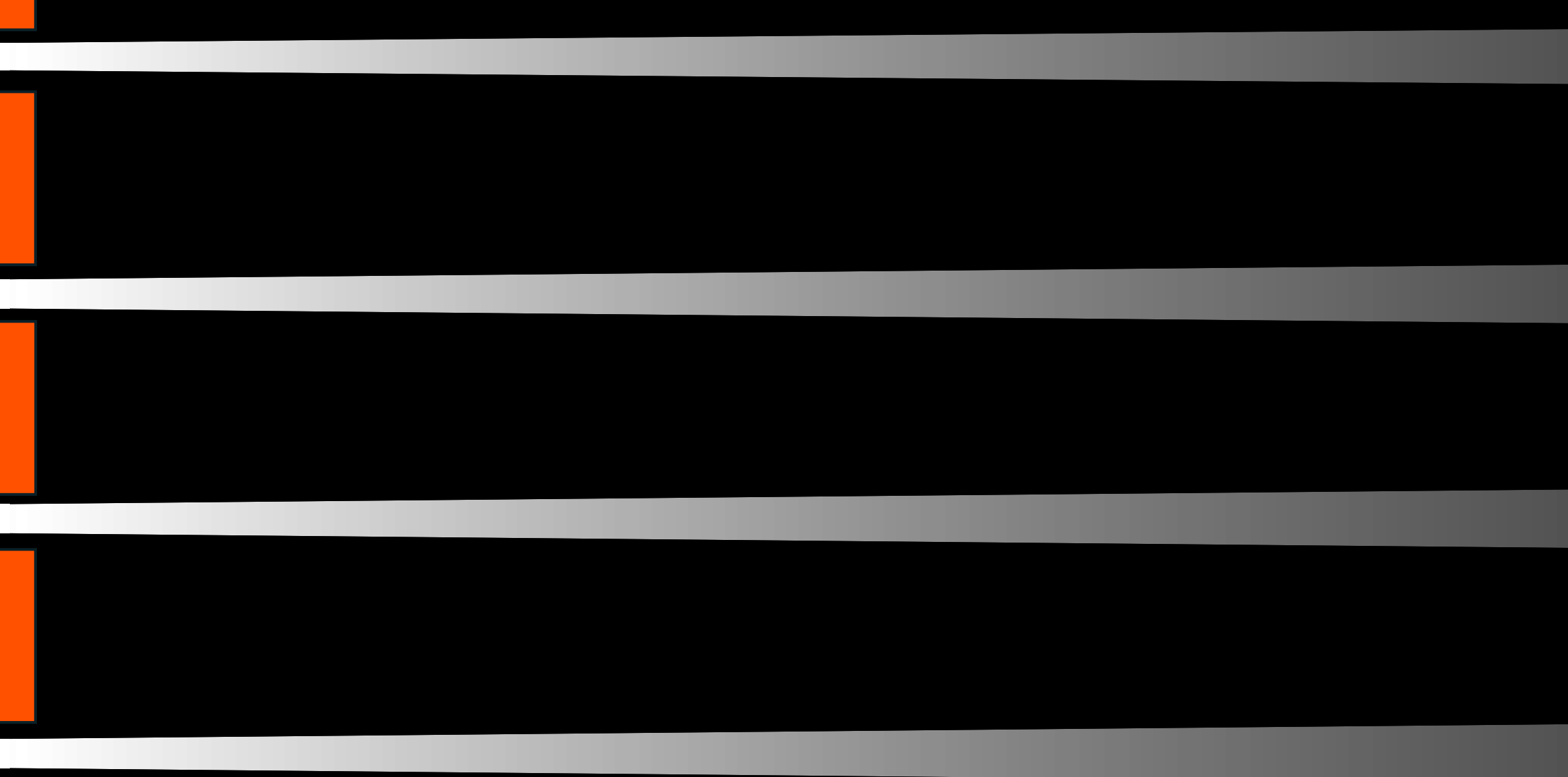
Edge Illumination

Phase

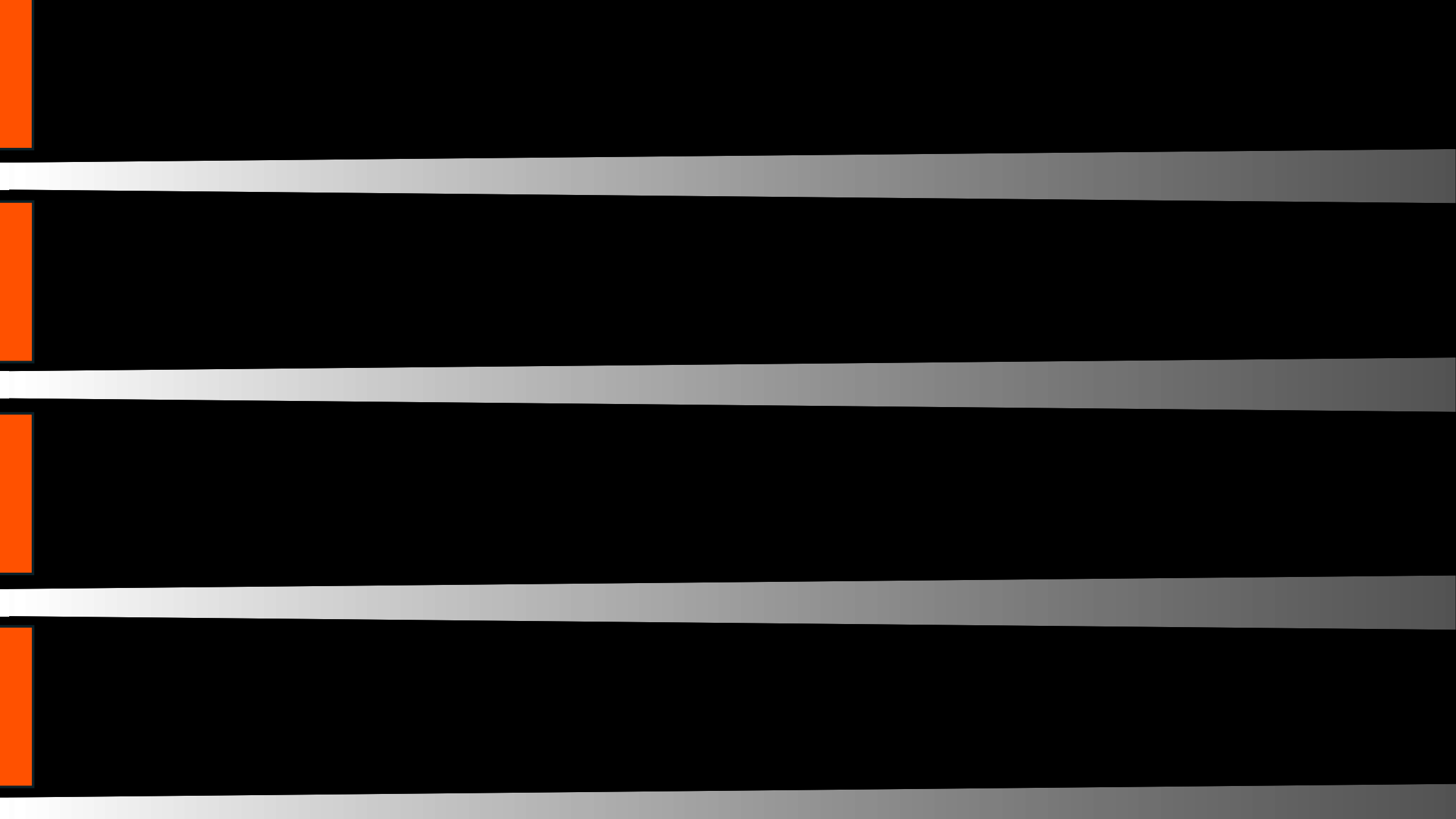
Contrast
Imaging



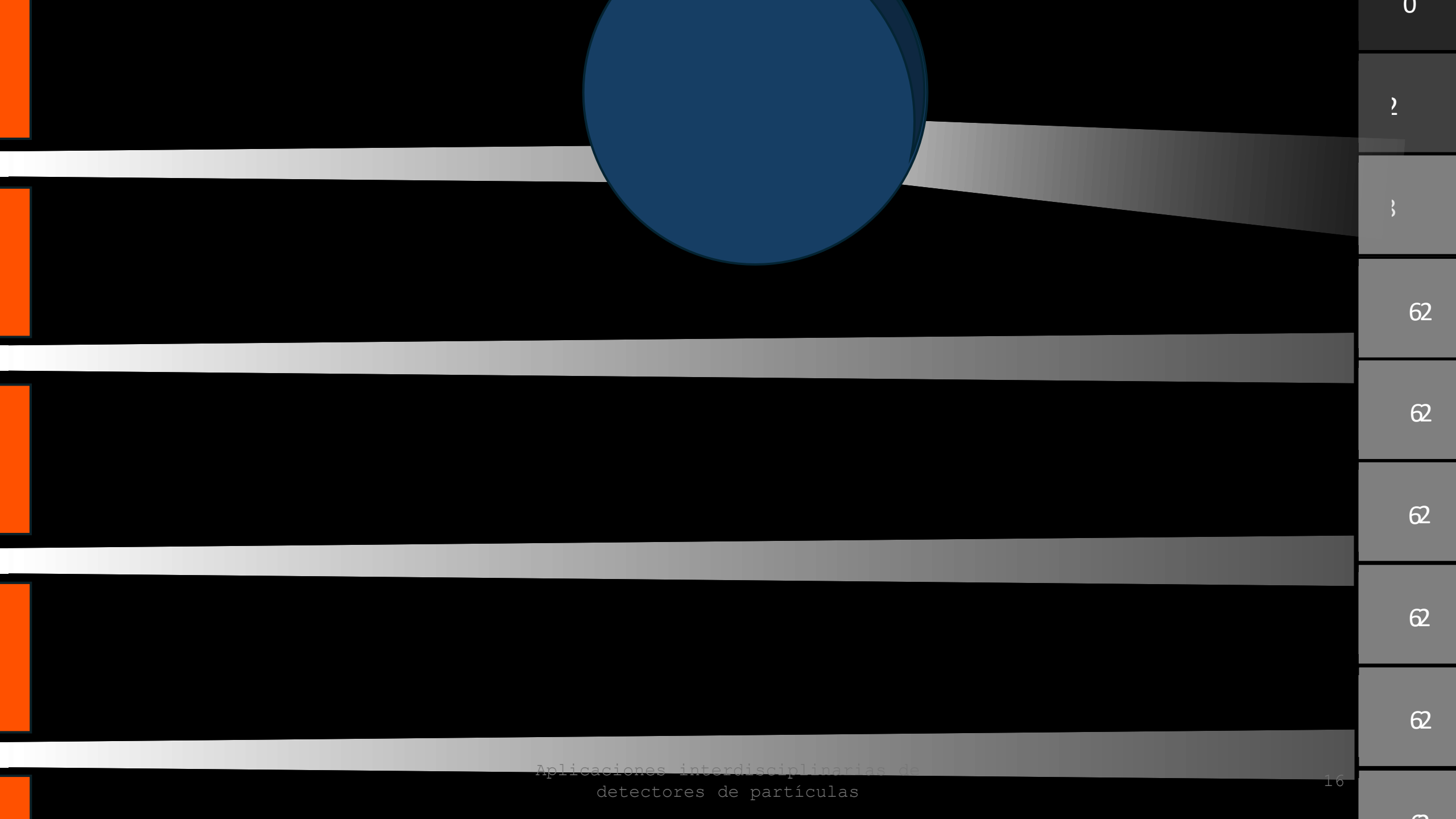


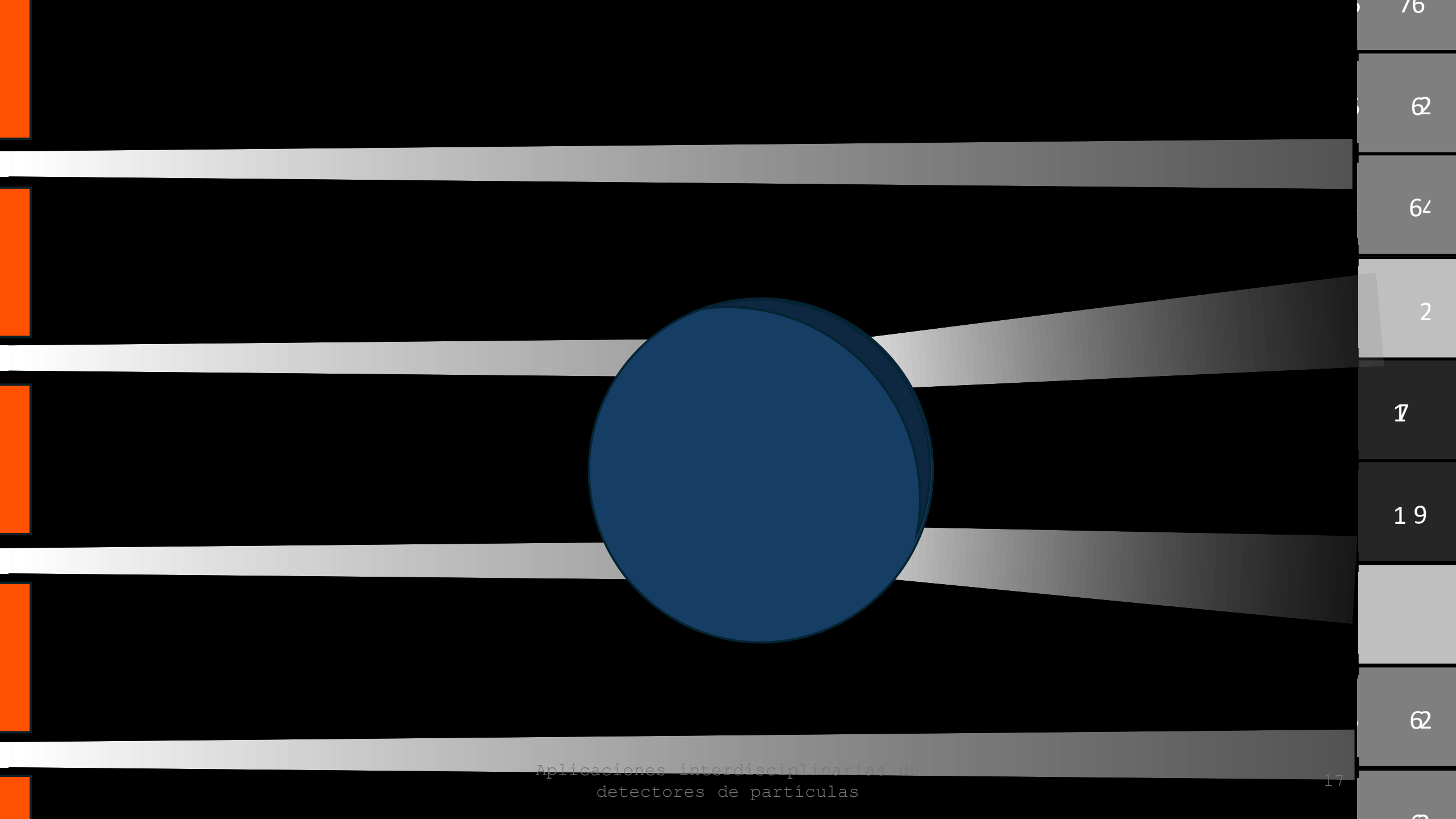


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Aplicaciones interdisciplinarias de
detectores de partículas

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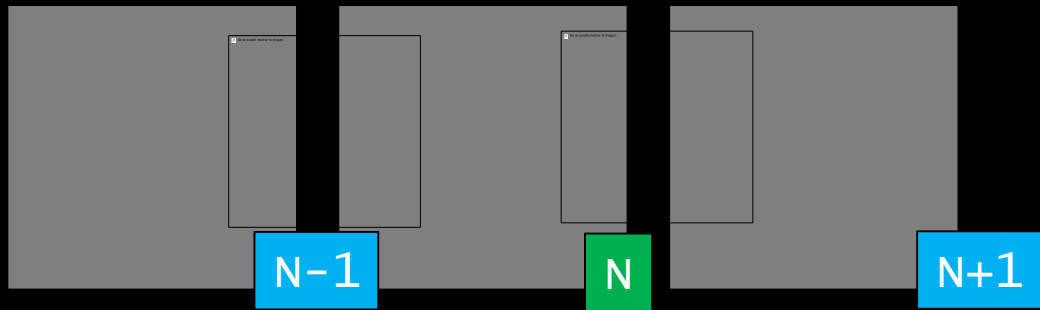
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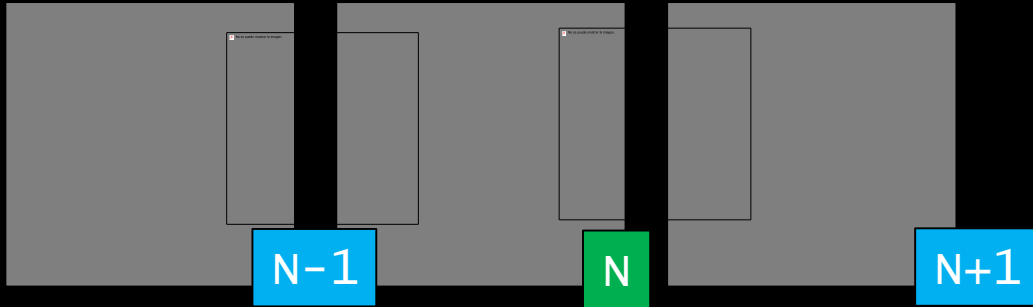
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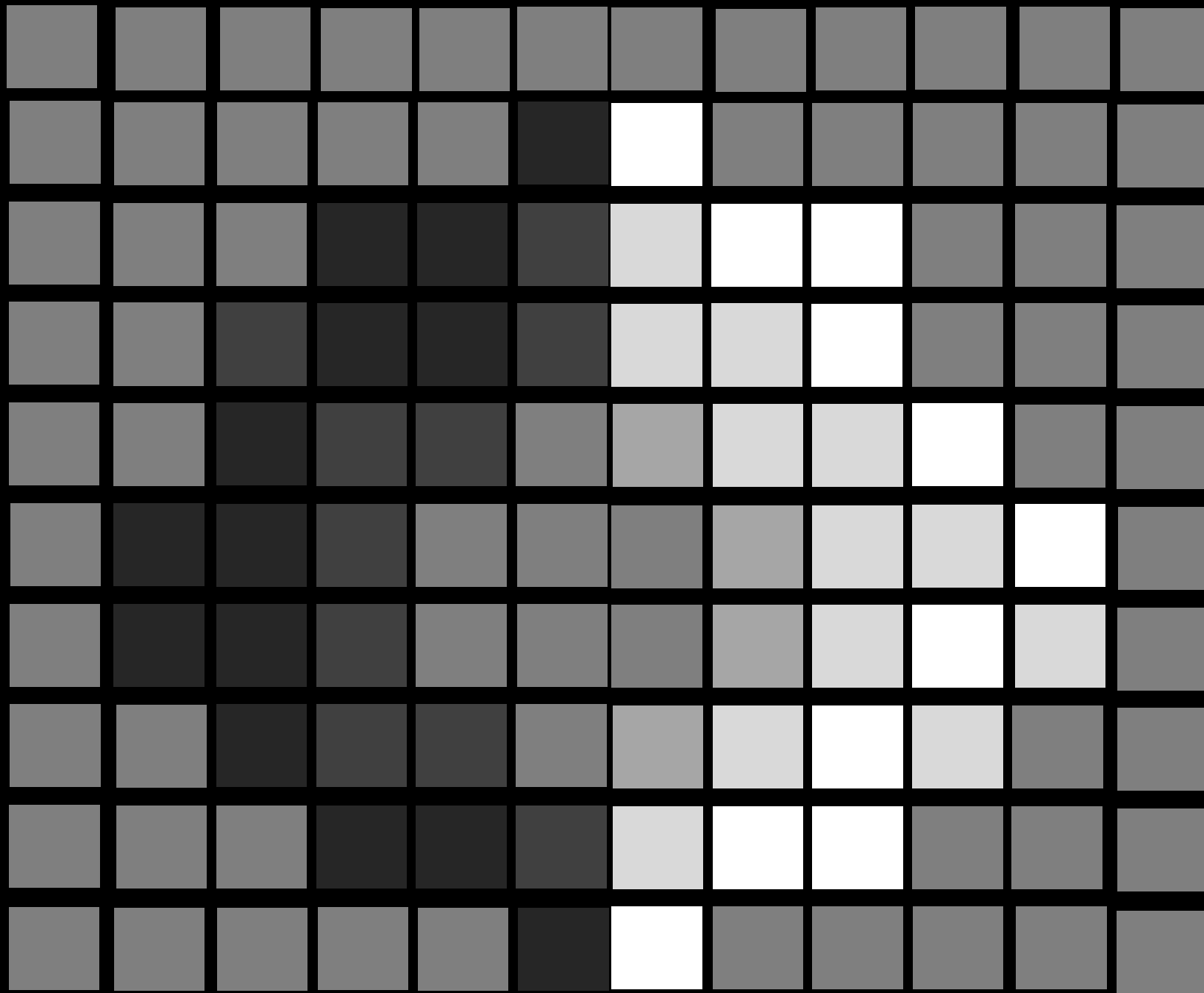
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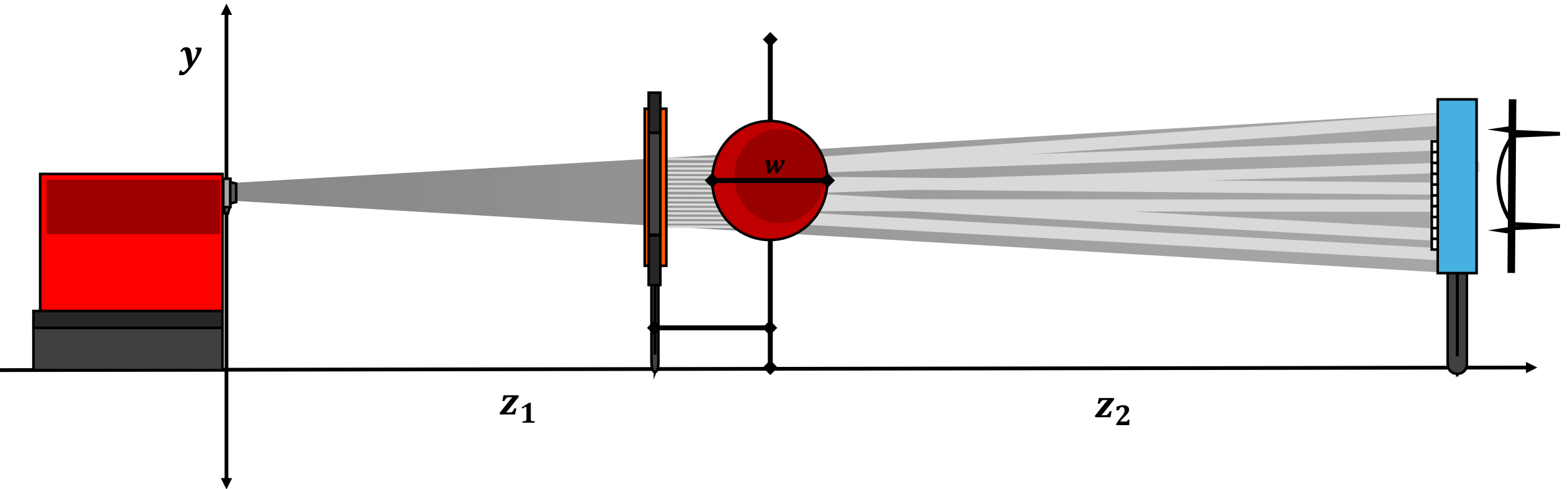


Aplicaciones industriales: líneas de
detectores de partículas

Can we make this
technology:

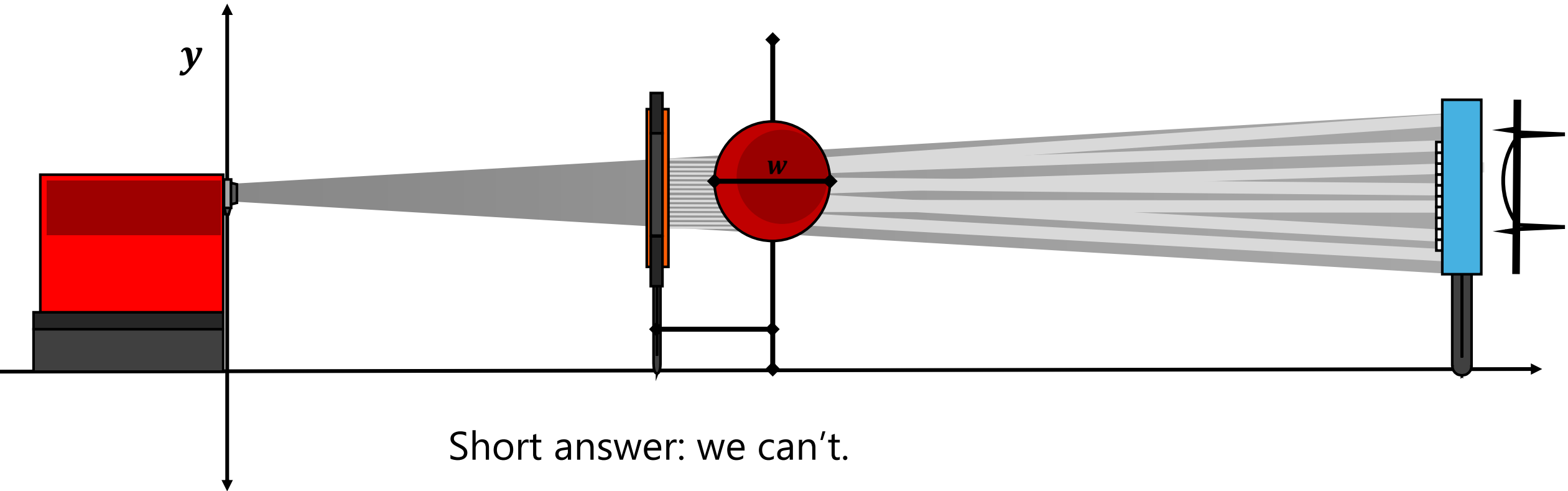
Universal Affordable

Universal



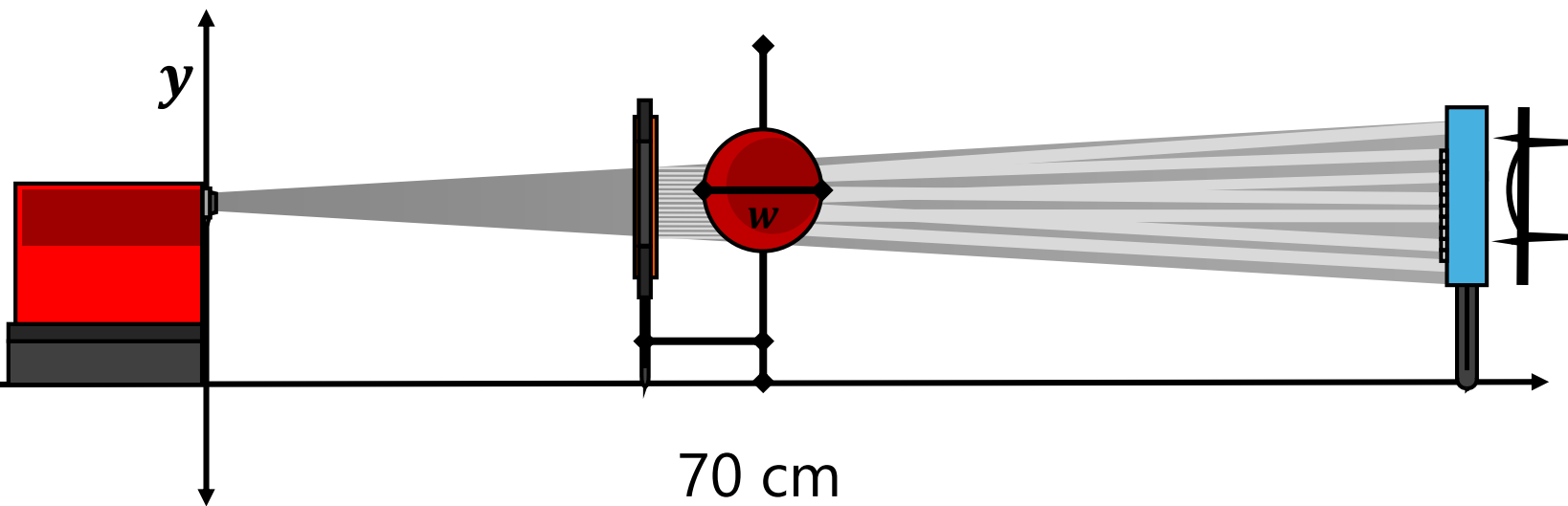
Universal

How do we apply this technique to any X-ray optical setup



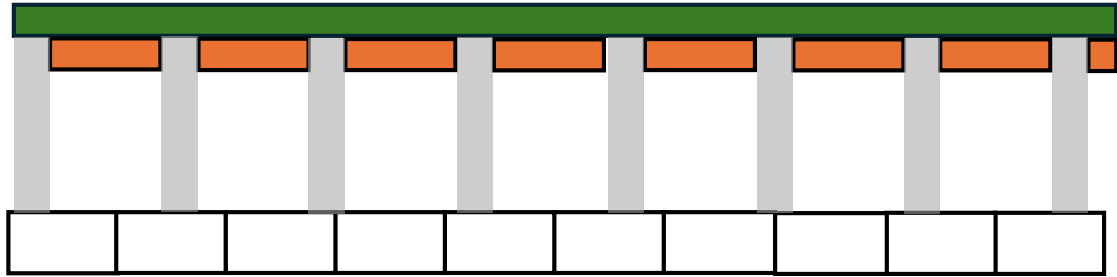
Short answer: we can't.

Universal

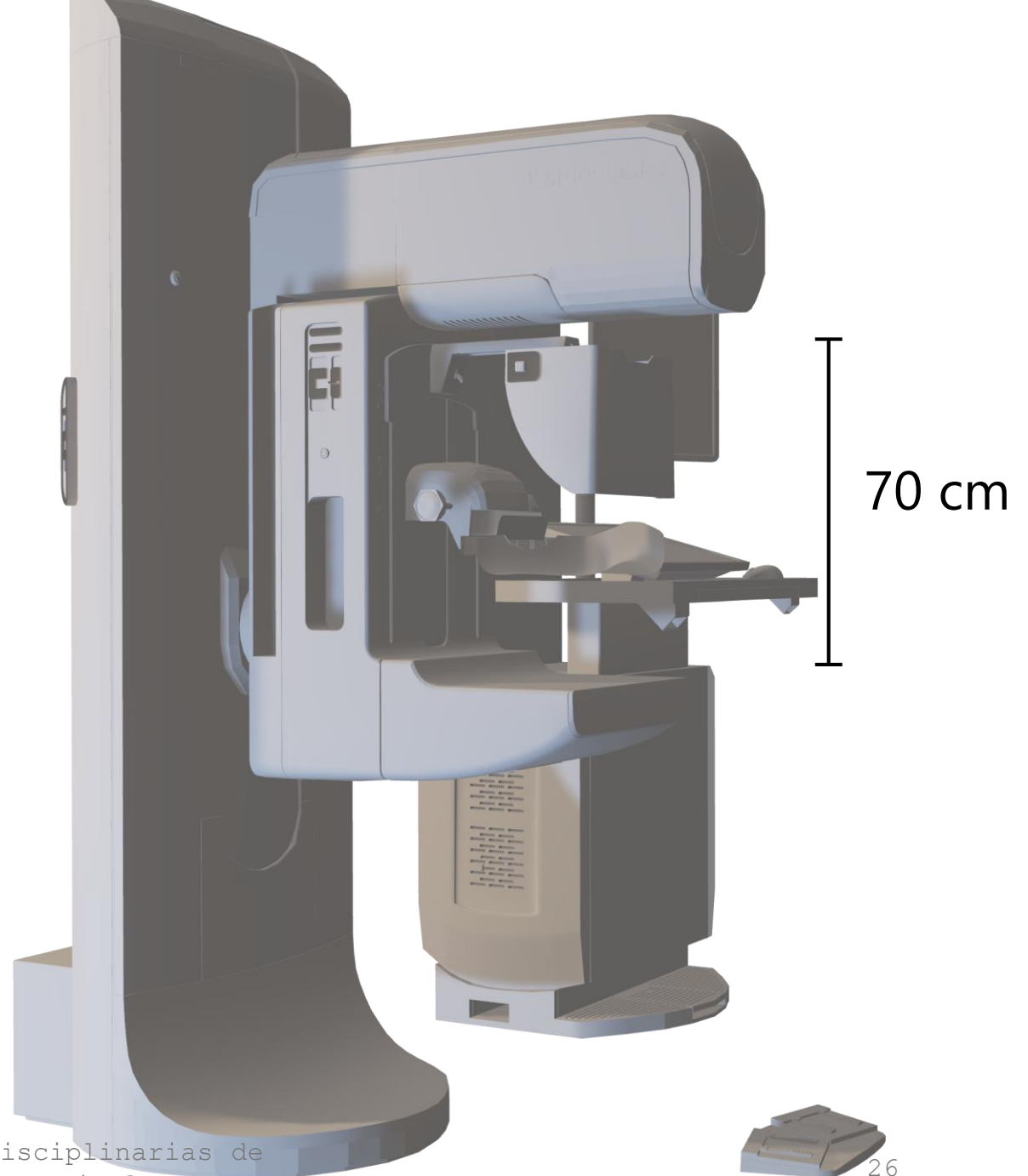


Aplicaciones interdisciplinarias de
detectores de partículas

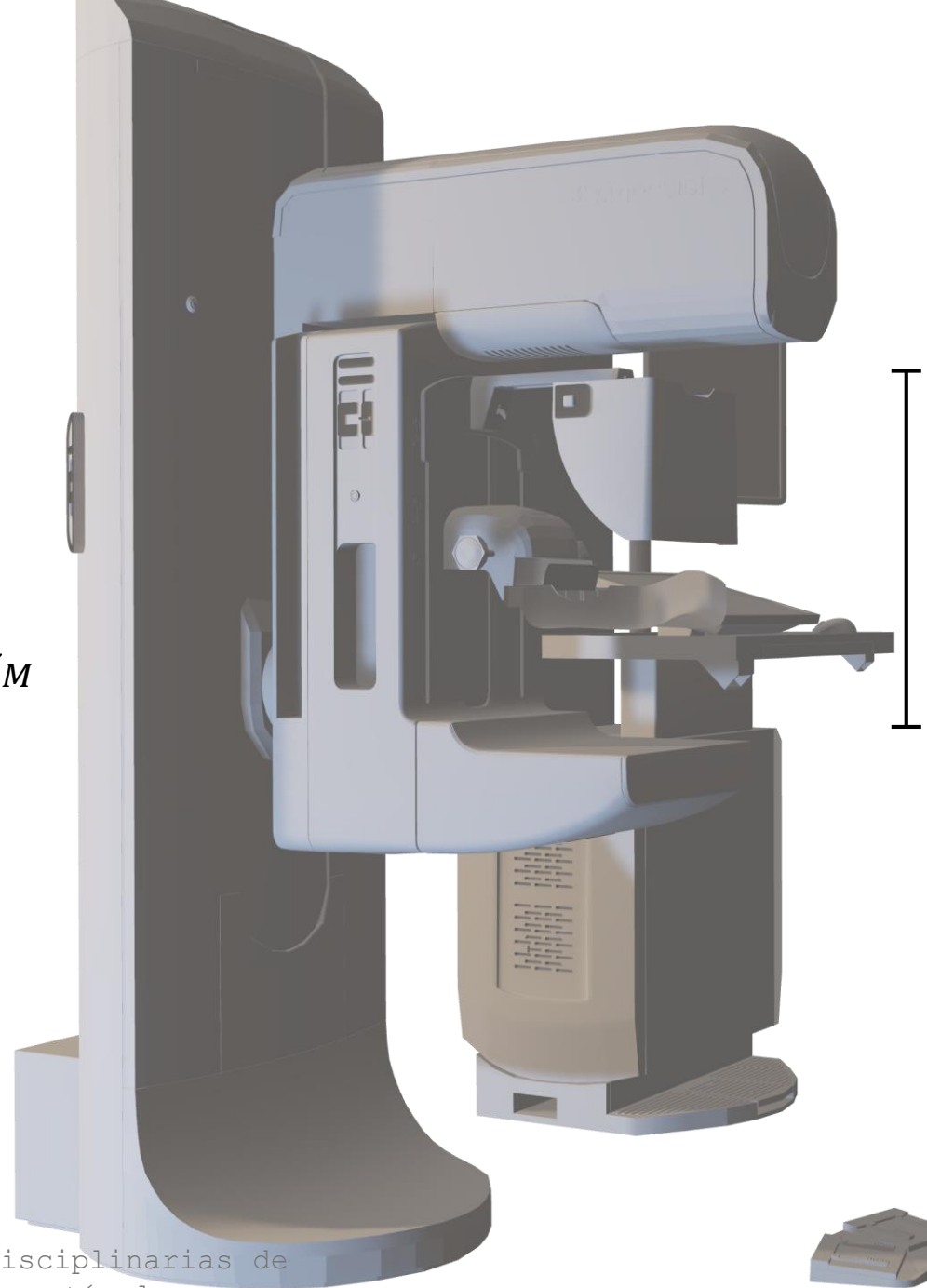
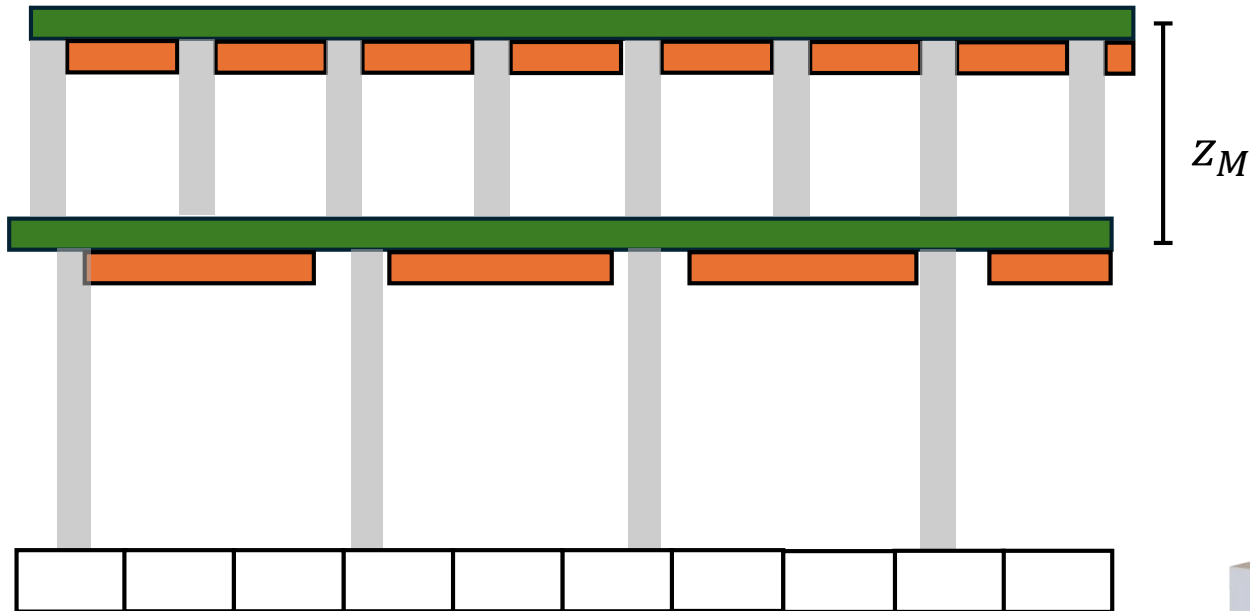
Universal



The wavefront marker must match detector pixel distribution given detector and distance (magnification) restrictions

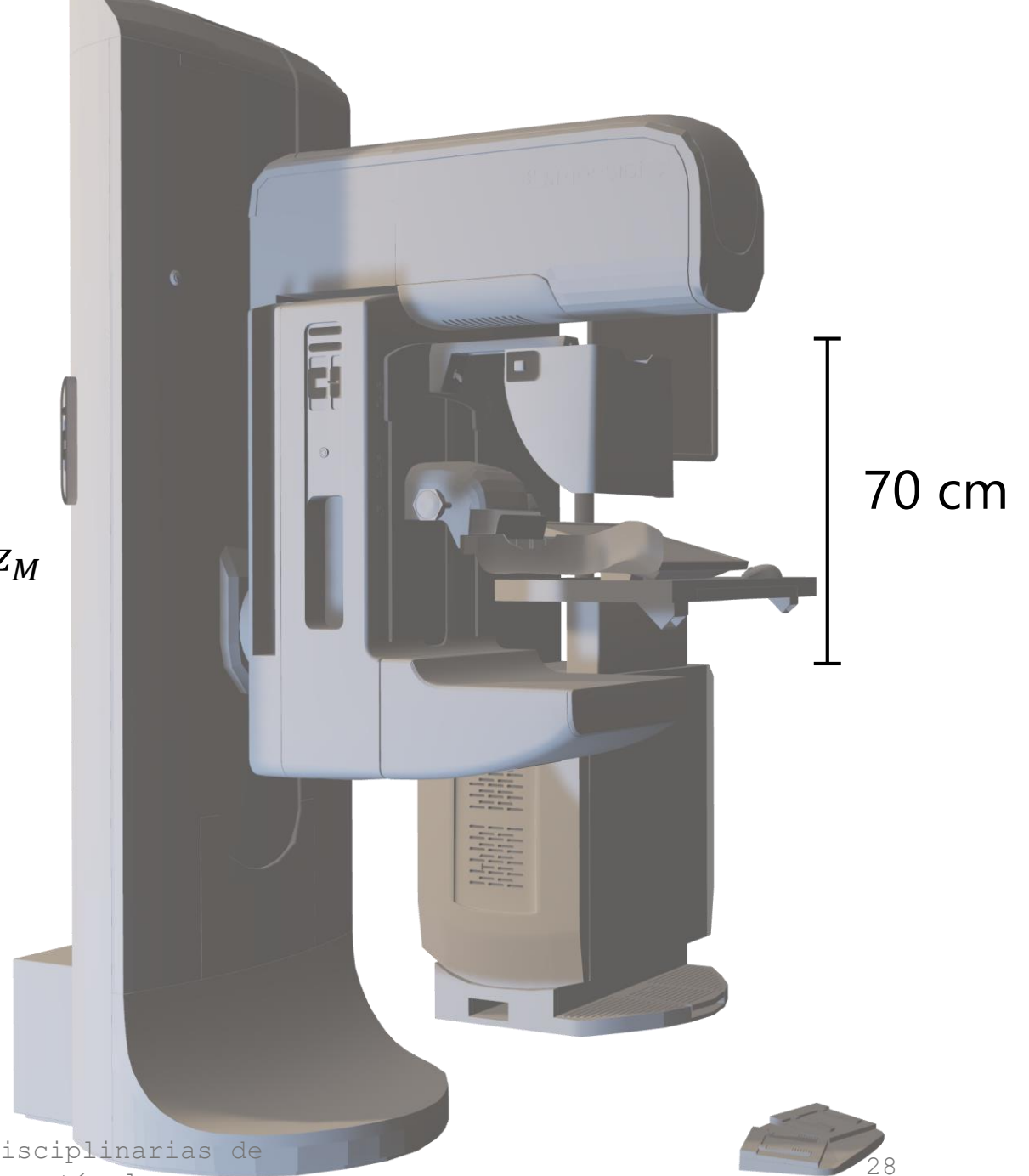
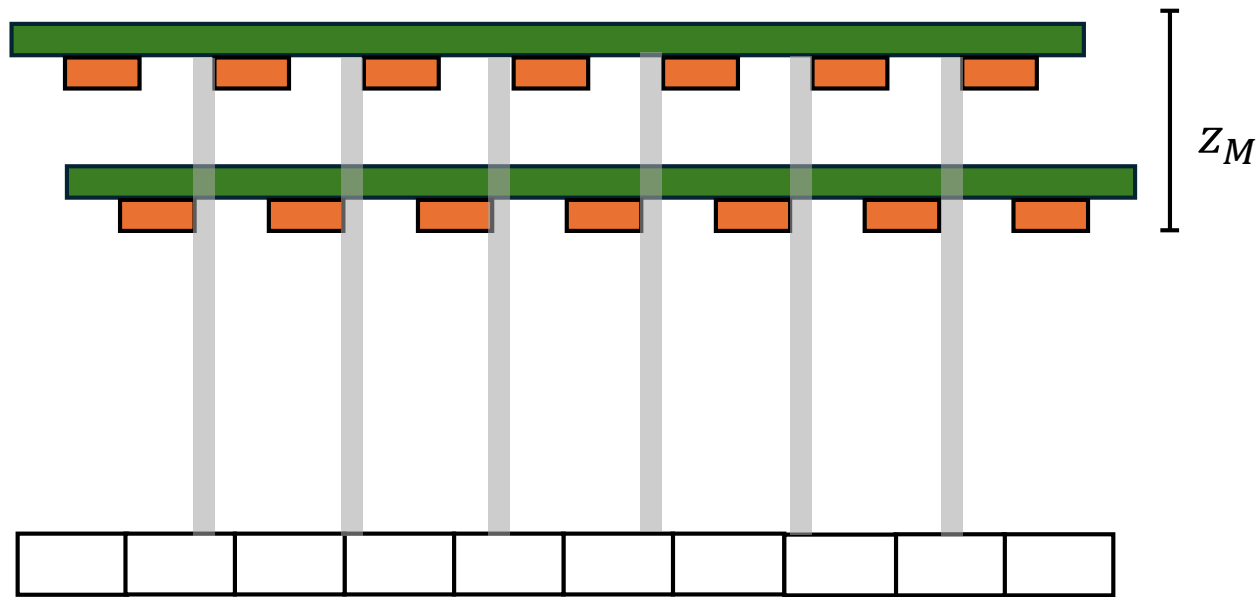


Universal



Aplicaciones interdisciplinarias de
detectores de partículas

Universal

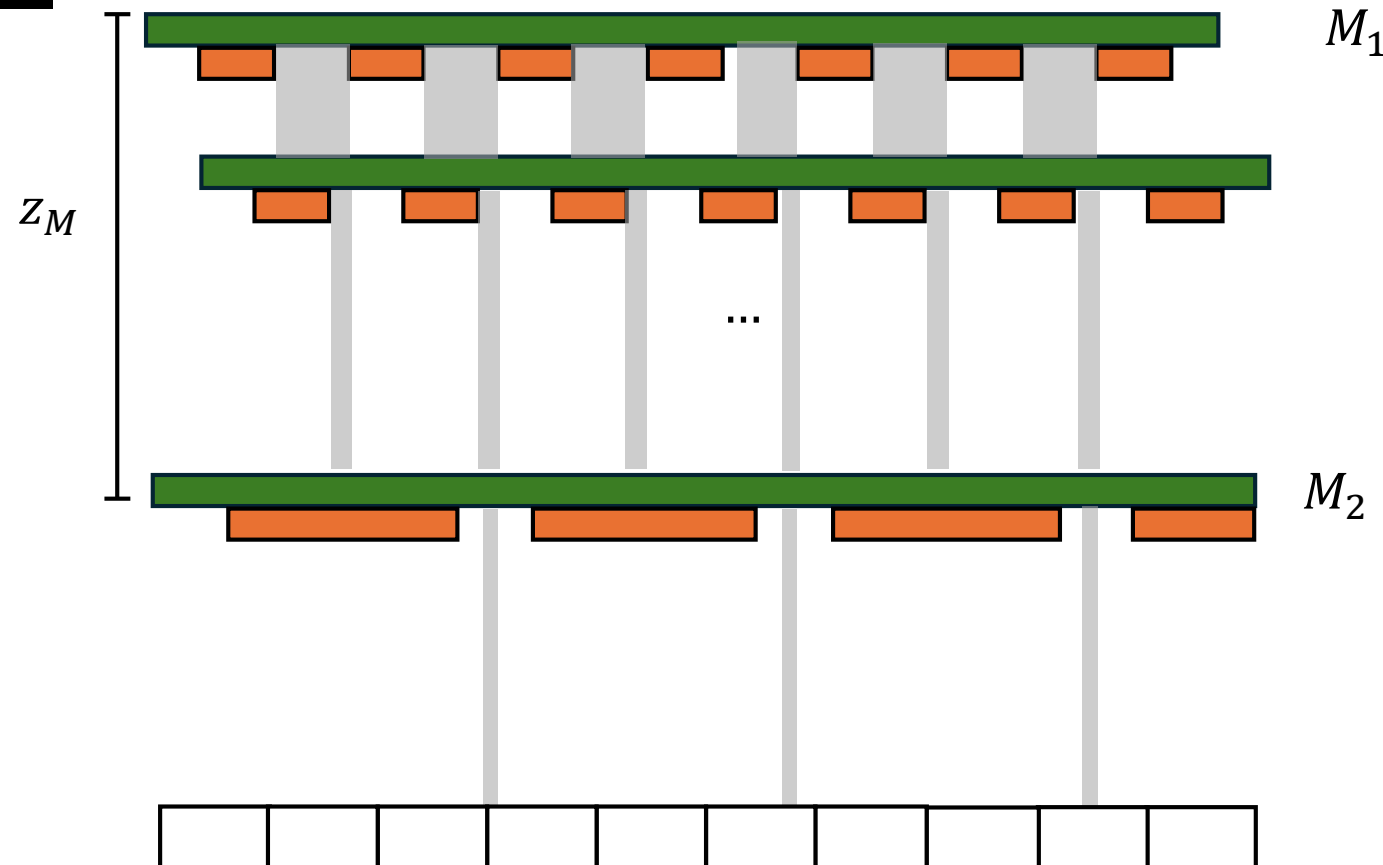


Aplicaciones interdisciplinarias de
detectores de partículas

Universal

As long as $z_M \ll z_{s-d}$ the wavefront markers can be operated as a single wavefront marker

$$M_1 * M_2 * \dots * M_n = \mathcal{M}$$



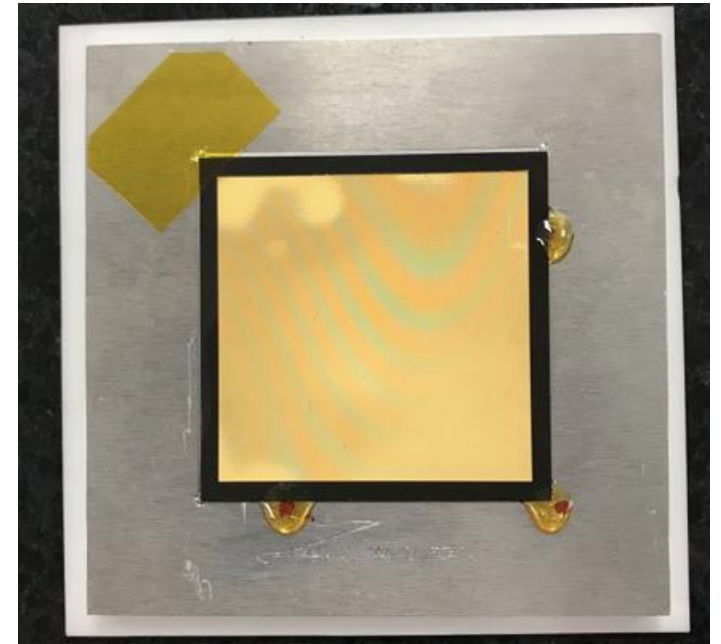
Affordable

Photolithography

Top quality material, maximizes DF-DPC sensibility

Sub-pixel resolution for most detectors

Few imperfections



Aplicaciones interdisciplinarias de
detectores de partículas

8k – 10k USD

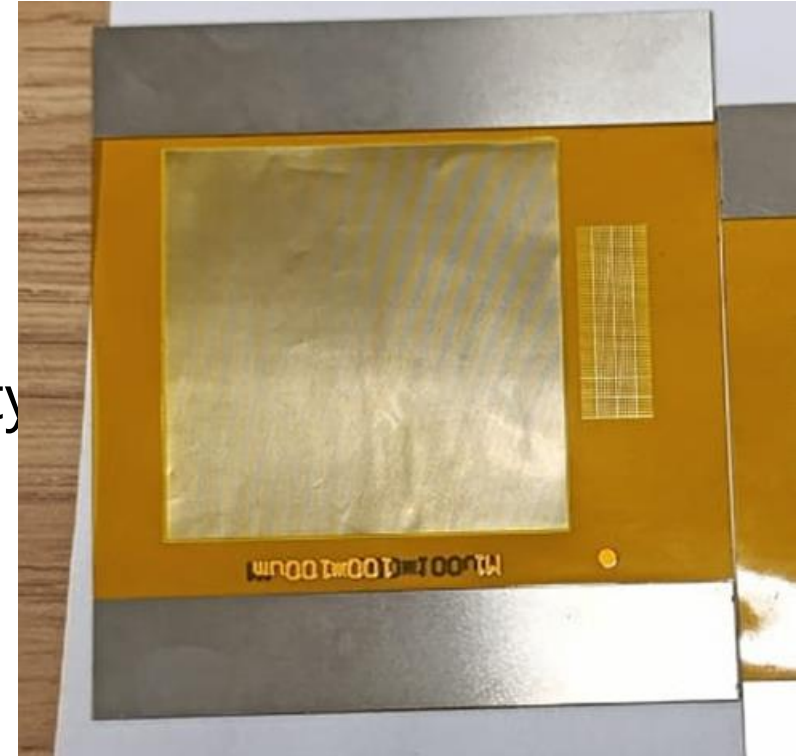
Affordable

PCB printing

Decent quality, acceptable DF-DPC sensibility

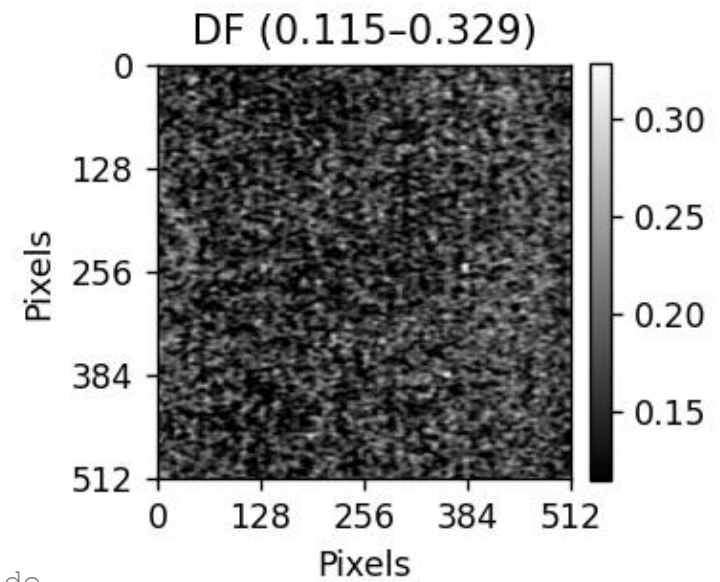
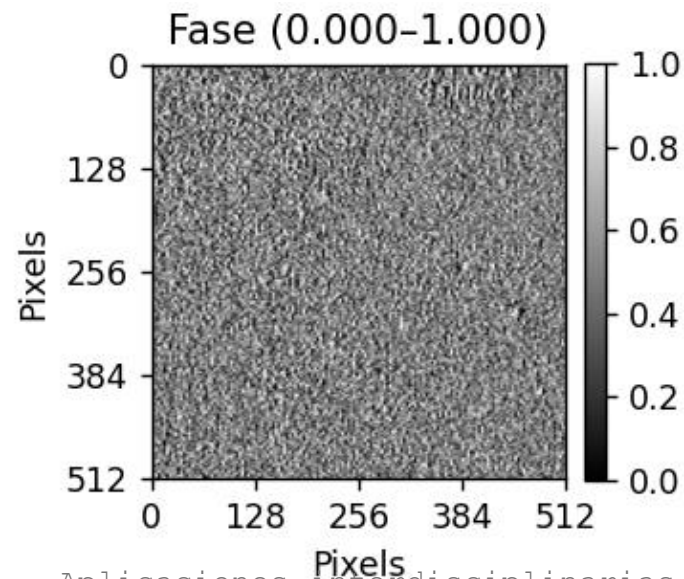
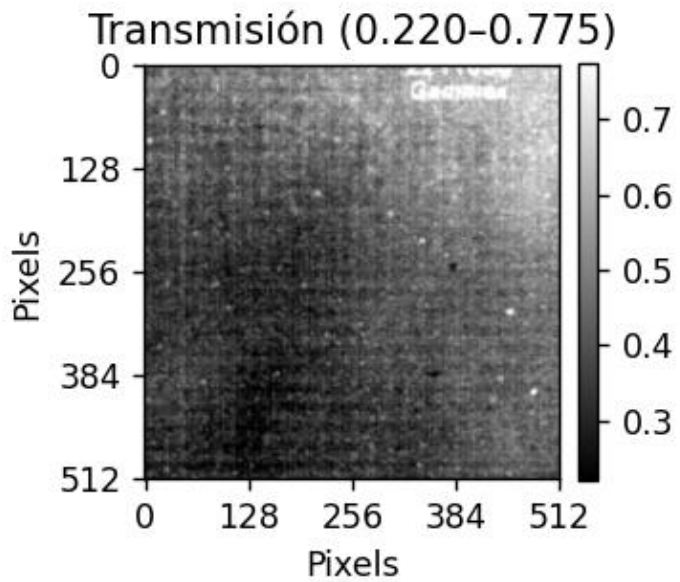
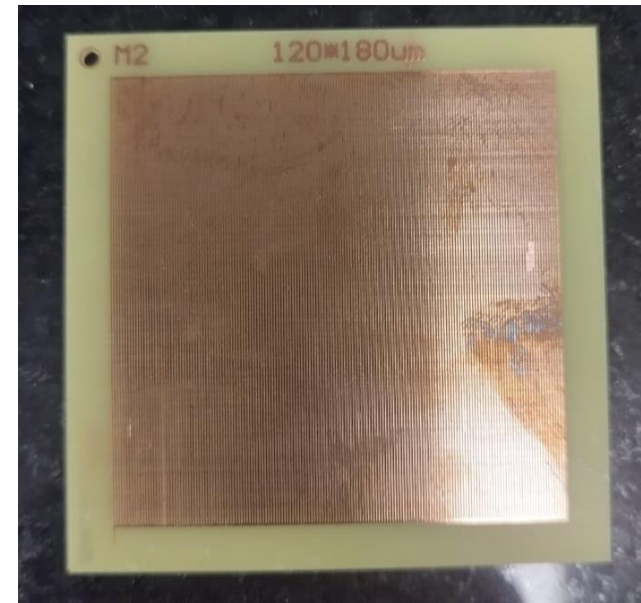
Conventional PCB printing $> 100\mu\text{m}$

Some imperfections

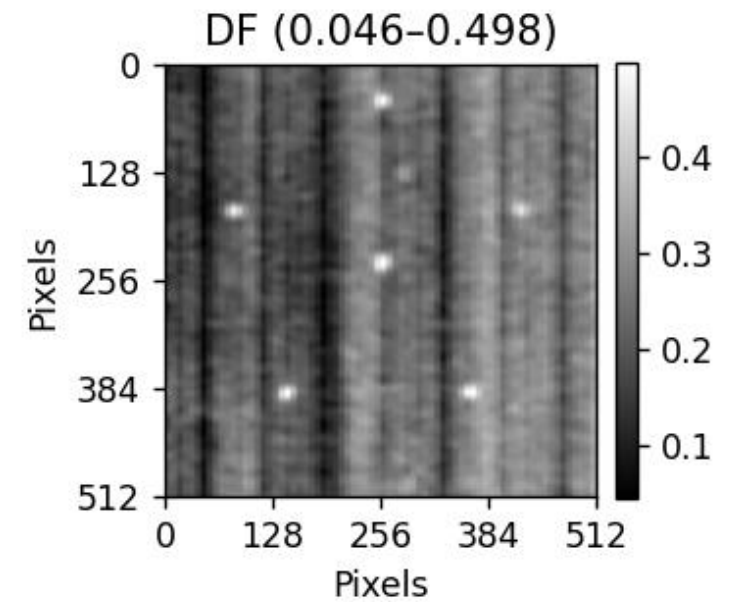
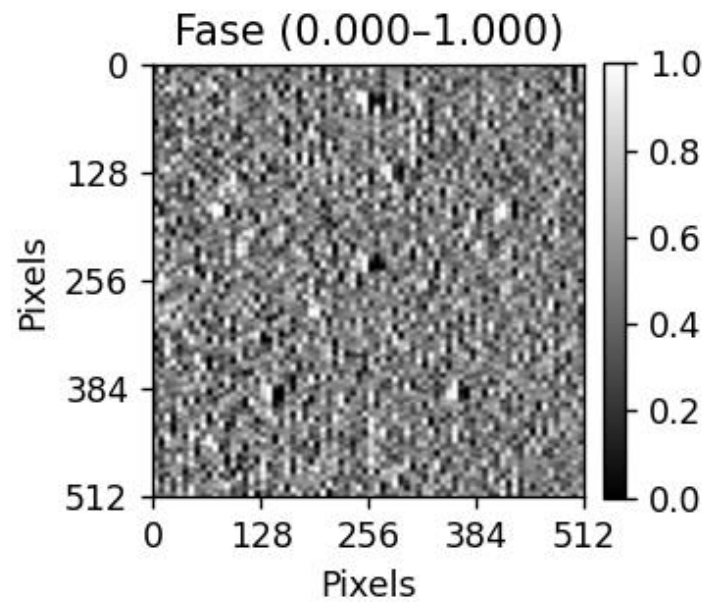
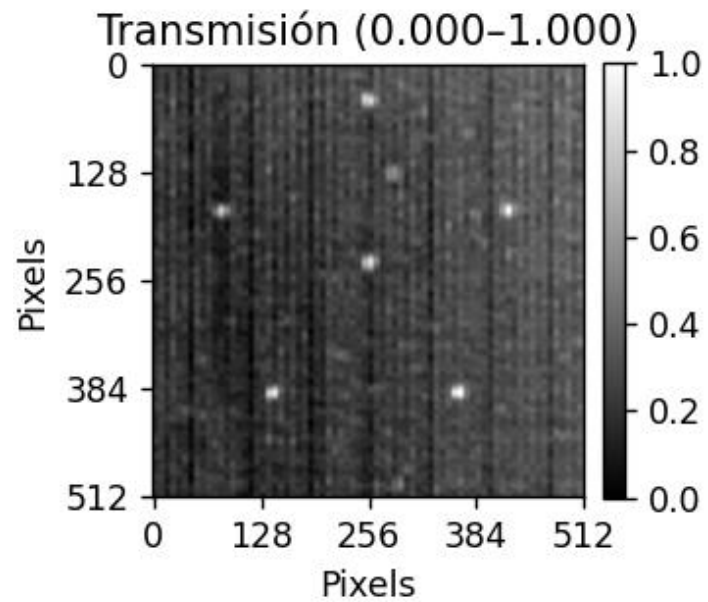
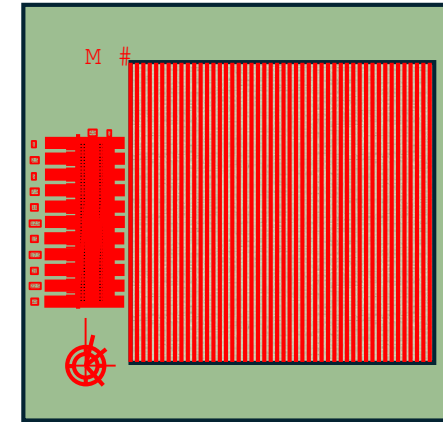


10 -14 USD

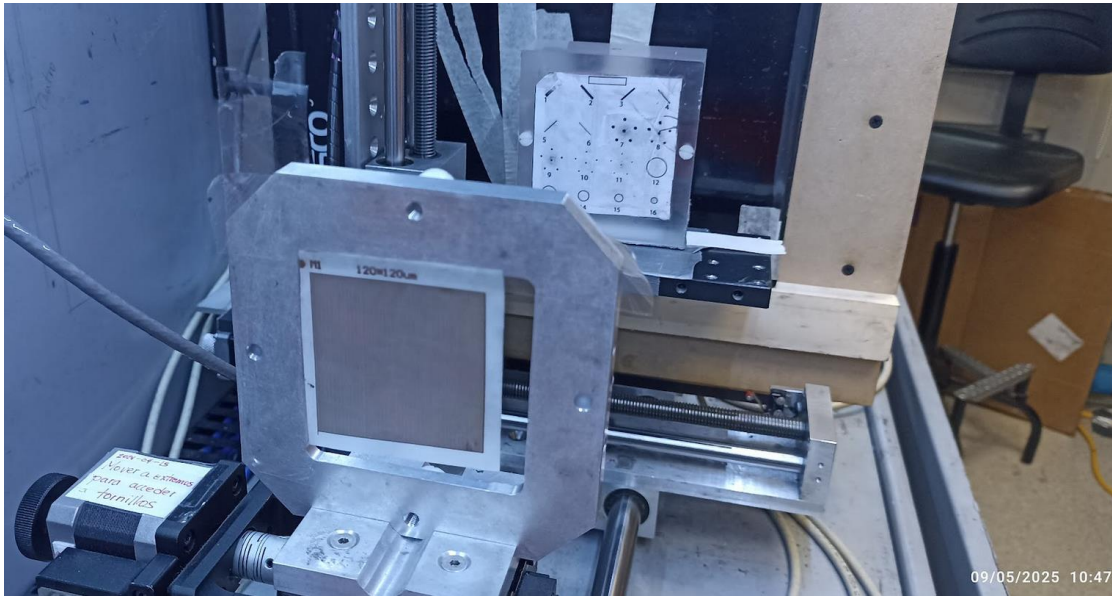
First prototype



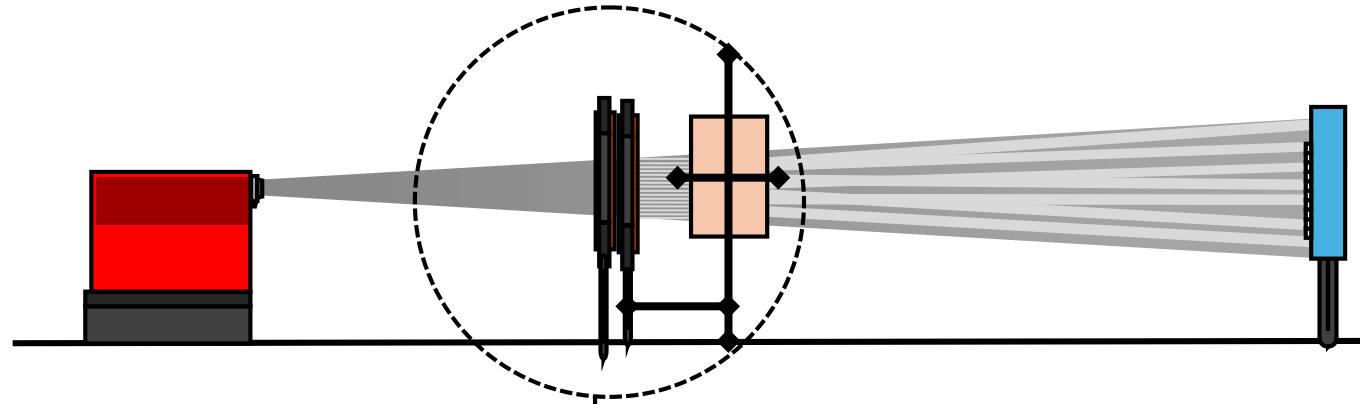
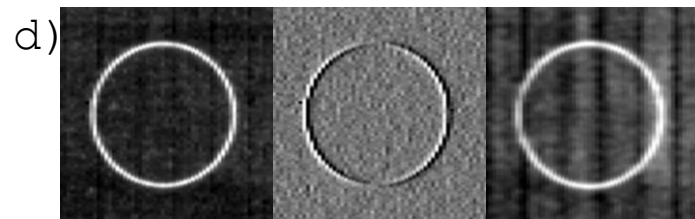
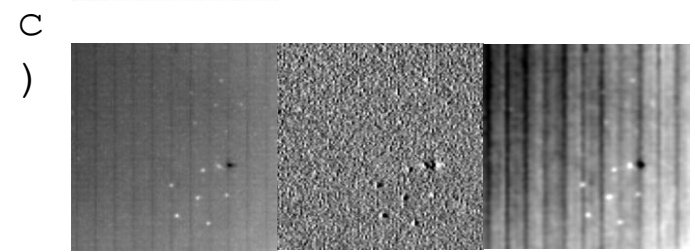
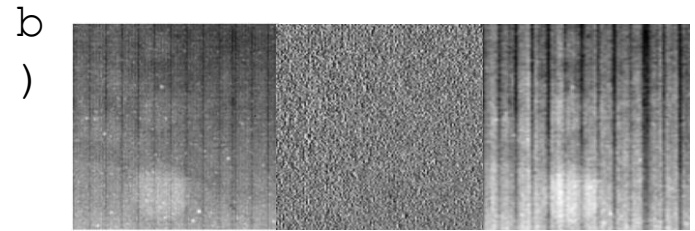
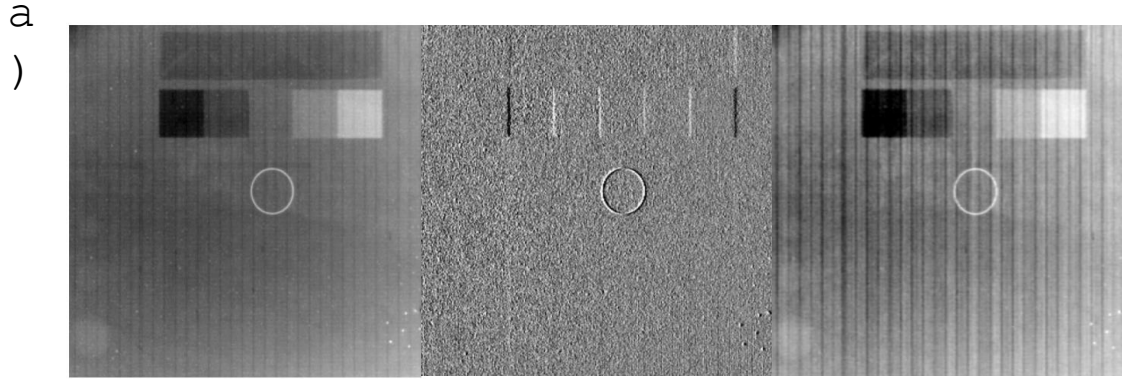
Second prototype



Third prototype



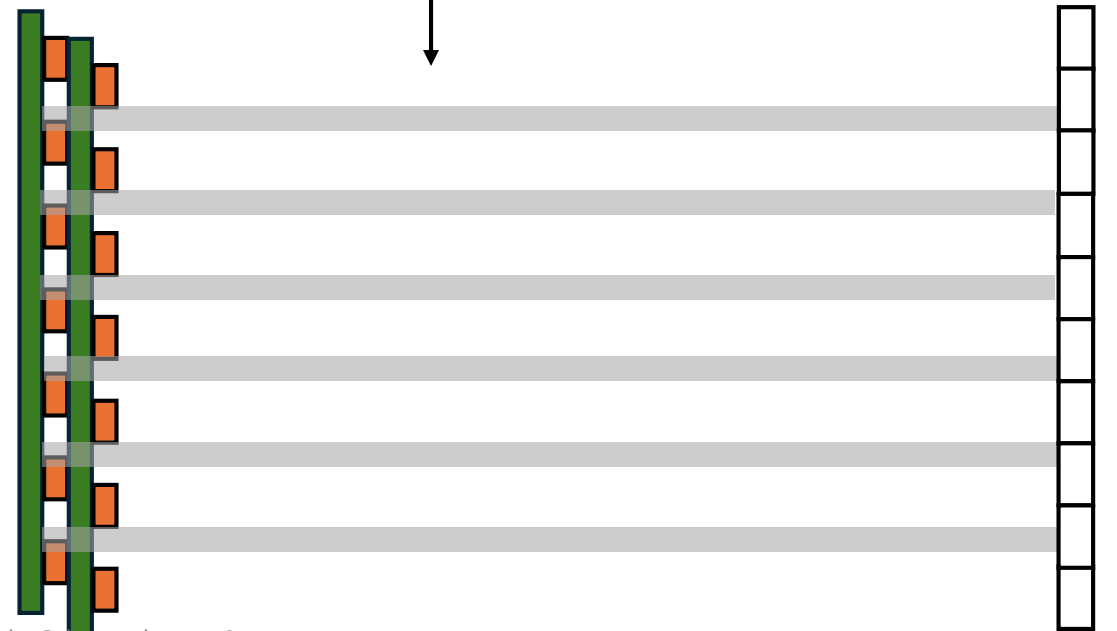
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detectores de partículas



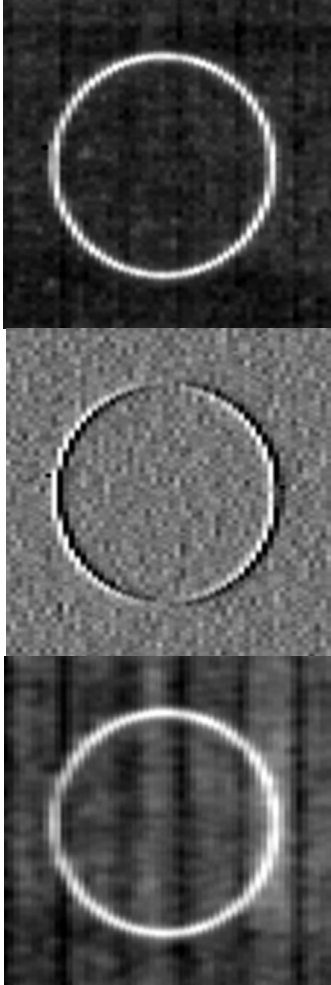
$$T_1 = T_2 = 200 \mu m$$

$$w_{1-2} \approx 40 \mu m$$

$$d = 143 \mu m$$



Retrieval method

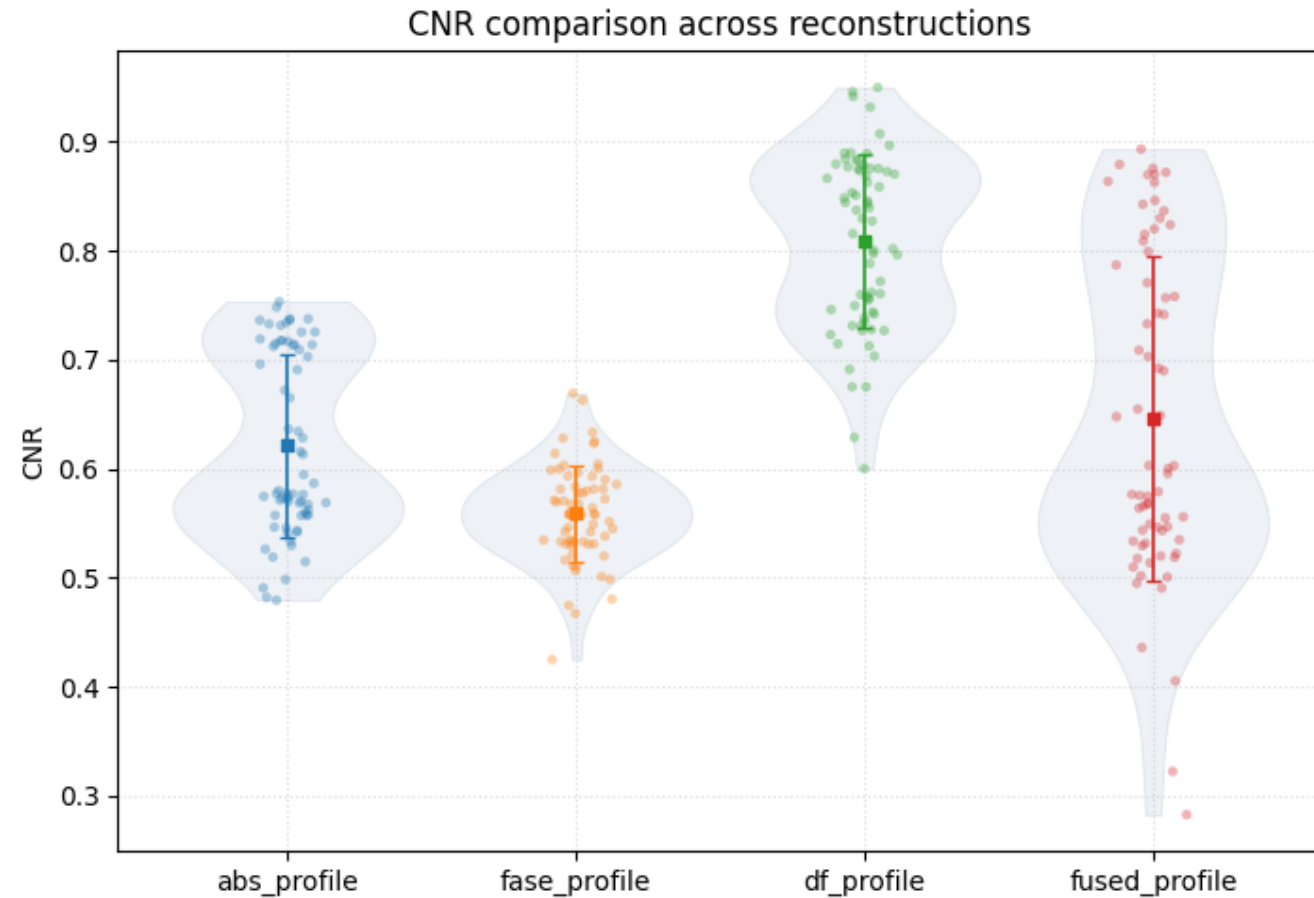
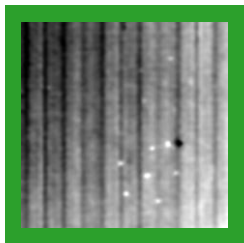
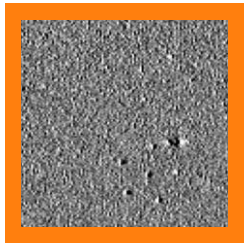
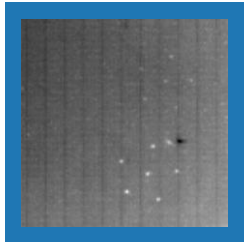


$$T_n(1 - L_n) = \frac{I_{n-1}^{(S)} + I_n^{(S)} + I_{n+1}^{(S)}}{I_{n-1}^{(M)} + I_n^{(M)} + I_{n+1}^{(M)}}$$

$$\frac{2\alpha_2}{w_e + \frac{1}{2}\alpha_1} D_n = \left(\frac{I_{n-1}^{(S)}}{I_{n-1}^{(M)}} - \frac{I_n^{(S)}}{I_n^{(M)}} \right) \frac{I_{n-1}^{(M)} + I_n^{(M)} + I_{n+1}^{(M)}}{I_{n-1}^{(S)} + I_n^{(S)} + I_{n+1}^{(S)}}$$

$$\frac{2\alpha_3}{w_e + 2\alpha_1} S_n = \left[1 - \frac{I_{n-1}^{(S)} + I_n^{(S)} - I_{n+1}^{(S)}}{I_{n-1}^{(M)} + I_n^{(M)} - I_{n+1}^{(M)}} \cdot \frac{I_{n-1}^{(M)} + I_n^{(M)} + I_{n+1}^{(M)}}{I_{n-1}^{(S)} + I_n^{(S)} + I_{n+1}^{(S)}} \right]$$

Do these masks work



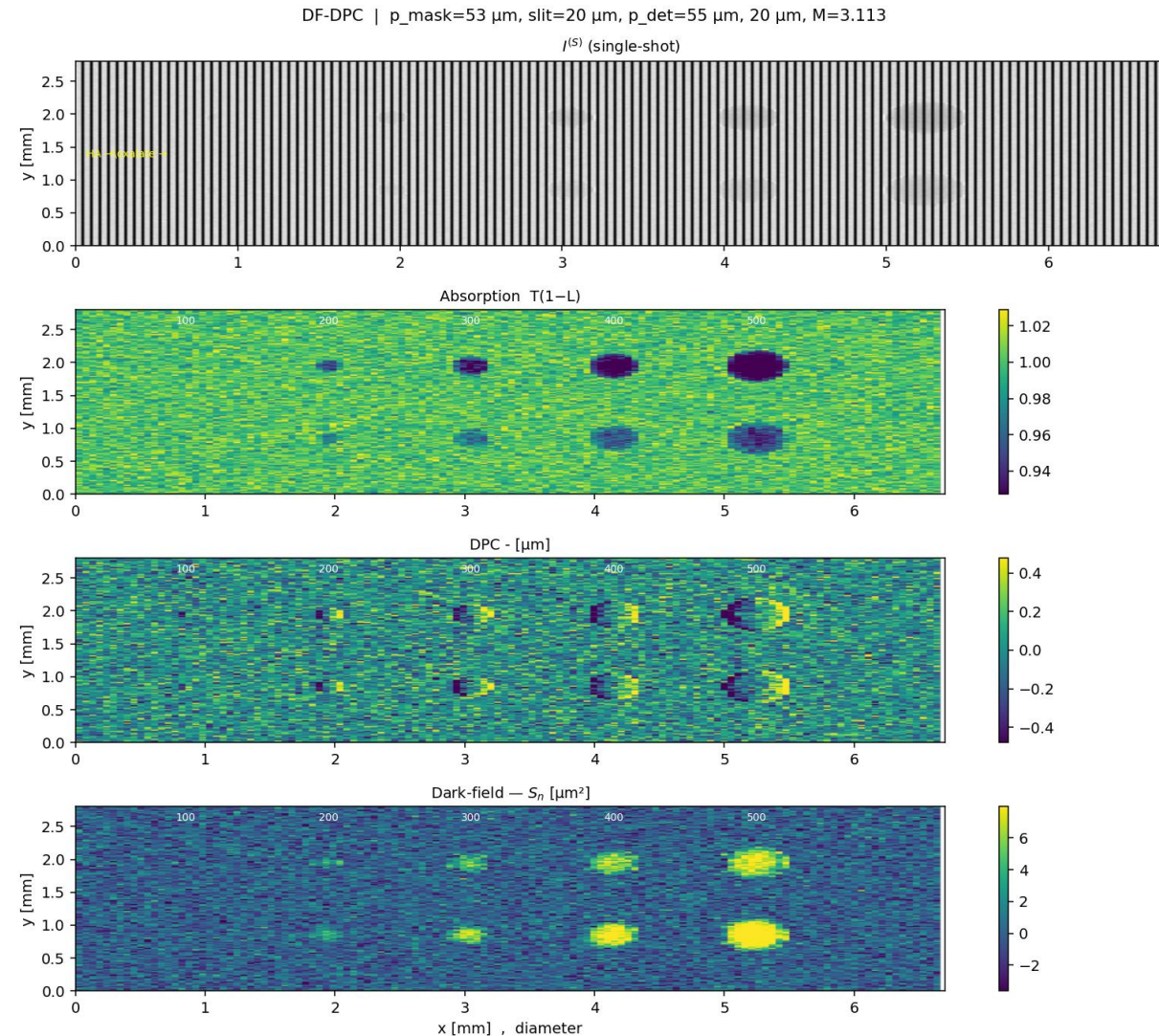
Final remarks

Mask modulation seems like a promising alternative to normalize DF-DPC imaging for several optical systems. Binning effects, dithering and artifacts are yet to be studied

PCB masks are a low-cost alternative that matches high-end photolithography masks for specific systems. A ground truth study is yet to be done to compare the effectiveness of PCB masks.

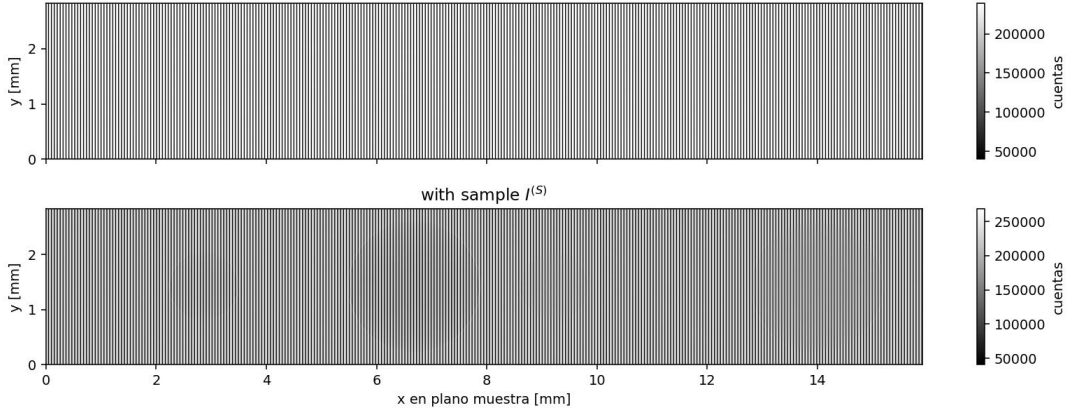
Bonus

This is a viable alternative for material classification (benign vs malignant microcalcifications)

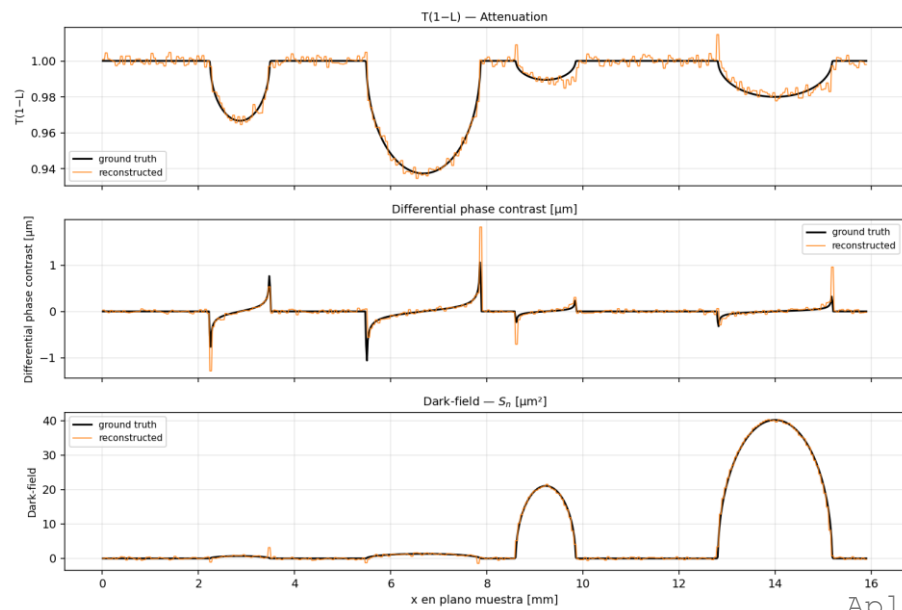


Detector images DF-DPC (M = 3.113)

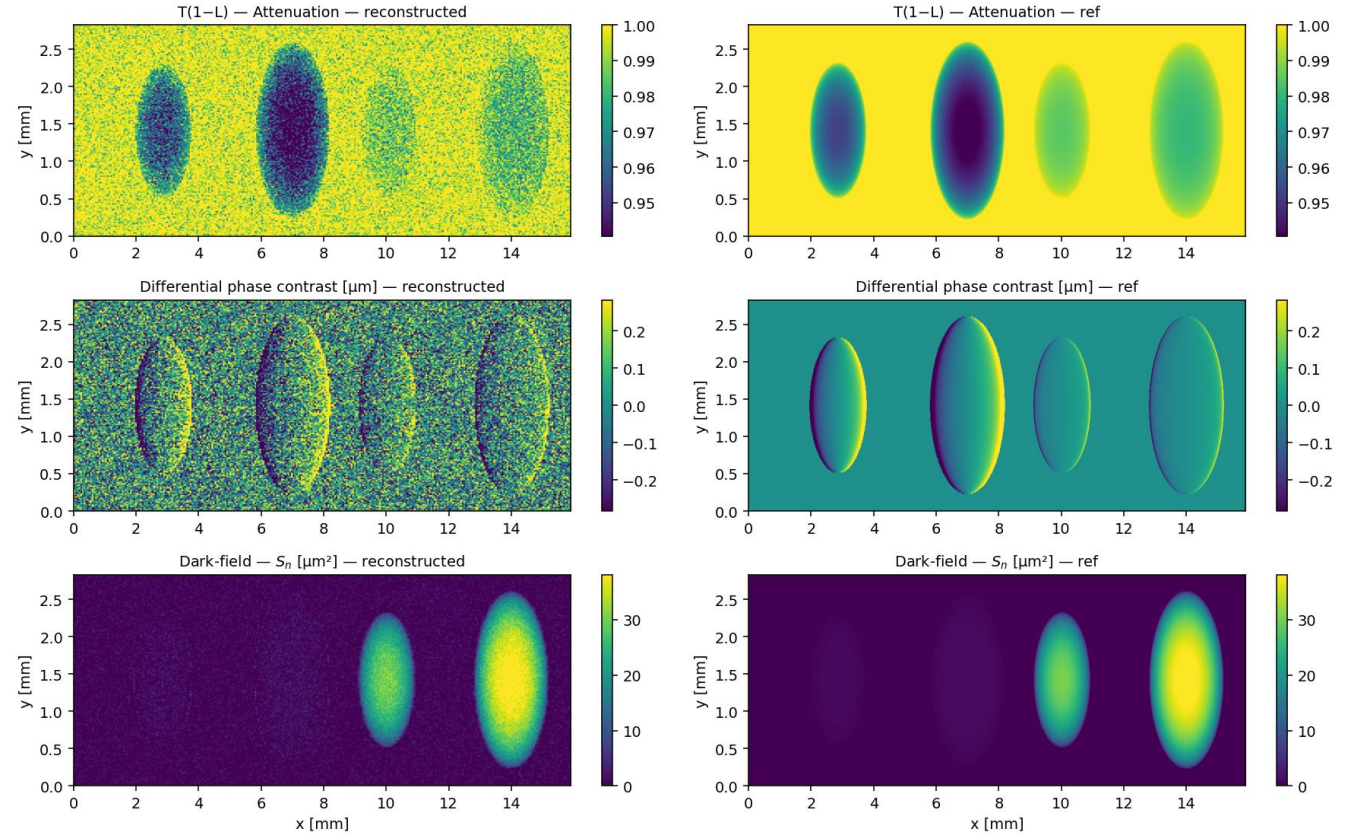
Reference with mask $I^{(M)}$



Perfiles centrales — configuración DF-DPC



single-shot reconstruction — DF-DPC



References

[1] Yuan, J., & Das, M. (2025). Single-shot, single-mask X-ray dark-field, and phase-contrast imaging. *Optica*, 12(12), 1895–1903.

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[2] Paganin, D. M., & Morgan, K. S. (2019). X-ray Fokker-Planck equation for paraxial imaging. *Scientific Reports*, 9, Article 17537.

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[3] Zuo, C., Li, J., Sun, J., Fan, Y., Zhang, J., Lu, L., Zhang, R., Wang, B., Huang, L., & Chen, Q. (2020). Transport of intensity equation: A tutorial. *Optics and Lasers in Engineering*, 135, Article 106187.

<https://doi.org/10.1016/j.optlaseng.2020.106187>